



Laplace Transform, Transfer Functions

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Chapter 2.3-2.5



Topics

■ **Review**

- Linearization through Taylor's Series approximation

■ **Today**

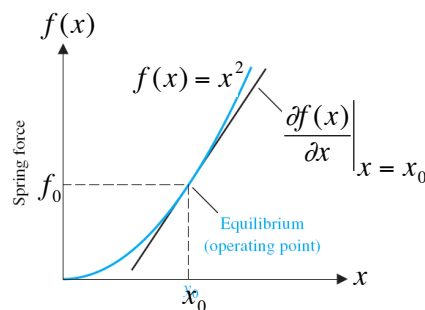
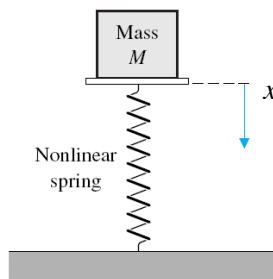
- Physical systems:
 - Spring-mass-damper system
 - RLC circuits
 - DC motor
- Laplace transform
- Transfer functions



How to Linearize

$$\Delta y = \left. \frac{\partial f(x)}{\partial x} \right|_{x=x_0} \Delta x$$

- Identify an operating point
- Perform Taylor series expansion and keep only constant and 1st derivative terms



Physical Laws of Process

■ For mechanical systems: Newton's laws

- Newton's second law of motion: the relationship between an object's mass **m**, its acceleration **a**, and the applied force **F**

$$\mathbf{F} = m\mathbf{a}$$

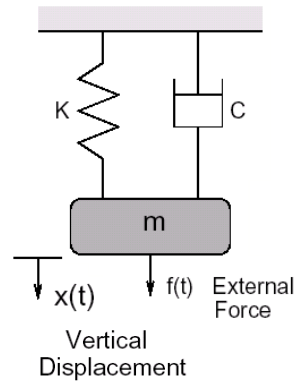
■ For electrical systems: Kirchhoff's laws

- 1st law or the *junction rule (KCL)*: For a given junction or node in a circuit, the sum of the currents entering equals the sum of the currents leaving.
- 2nd law or the *loop rule (KVL)*: Around any closed loop in a circuit, the sum of the potential differences across all elements is zero.



Spring-Mass-Damper System**

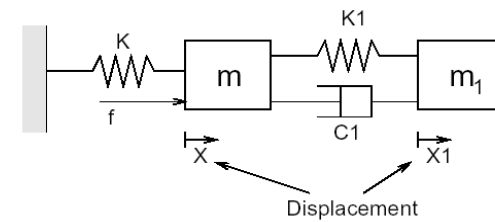
- $F(t)$: equivalent force on mass m
- The signs of $-kx$ and $-c\dot{x}$ are negative because these forces oppose the motion of $f(t)$



$$m\ddot{x} = F(t) = -kx - c\dot{x} + f(t)$$



Two-Mass System**

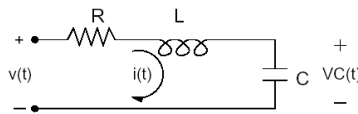


$$\begin{cases} m\ddot{x} = f(t) - Kx + K_1(x_1 - x) + C_1(\dot{x}_1 - \dot{x}) \\ m_1\ddot{x}_1 = -K_1(x_1 - x) - C_1(\dot{x}_1 - \dot{x}) \end{cases}$$

Assume the motion directions: $x > 0$; $x_1 - x > 0$



Series RLC Circuit**



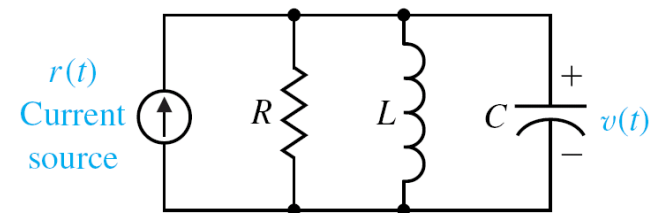
Applying Kirchhoff's voltage law yields an integro-differential model:

$$\begin{aligned} v(t) &= v_R(t) + v_L(t) + v_C(t) \\ &= Ri(t) + L\frac{di(t)}{dt} + \frac{1}{C} \int_0^t i(\tau) d\tau \end{aligned}$$

Input: $v(t)$; Output: $i(t)$



Parallel RLC Circuit**



Applying Kirchhoff's current law:

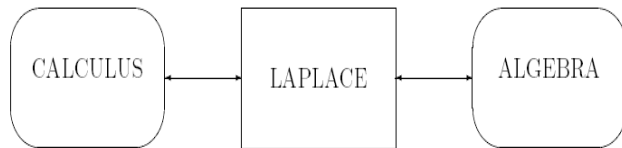
$$C \frac{dv(t)}{dt} + \frac{1}{R}v(t) + \frac{1}{L} \int_0^t v(\tau) d\tau = r(t)$$

Input: $r(t)$; Output: $v(t)$



The Laplace Transform

- The method of Laplace transforms converts a calculus problem (the linear differential equation) into an algebra problem.
- The solution of the algebra problem is then fed backwards through a the *Inverse Laplace Transform* and the solution to the differential equation is obtained.



The Laplace Transform



- Pierre-Simon Laplace (1749-1827)
- Laplace proved the stability of the solar system. He also put the theory of mathematical probability on a sound footing
- "All the effects of Nature are only the mathematical consequences of a small number of immutable laws."
- Studied, but did not fully developed the Laplace transform



The Laplace Transform

- Like the Fourier transform, the Laplace transform is an *integral transform*

$$\mathcal{L}[f(t)](s) = \int_0^{\infty} f(t)e^{-st} dt$$

- Alternately the Laplace variable s can be considered to be the differential operator:

$$s = \frac{d(\cdot)}{dt}$$



Laplace Transform Properties

- Linearity:

$$\begin{aligned} \mathcal{L}[kf(t)] &= kF(s) \\ \mathcal{L}[f_1(t) + f_2(t)] &= F_1(s) + F_2(s) \end{aligned}$$

- Differentiation:

$$\begin{aligned} \mathcal{L}[\dot{f}(t)] &= sF(s) - f(0^-) \\ \mathcal{L}[\ddot{f}(t)] &= s^2F(s) - s\dot{f}(0^-) - \dot{f}(0^-) \\ \mathcal{L}[f^{(n)}(t)] &= s^nF(s) - s^{n-1}f(0^-) - \dots - f^{(n-1)}(0^-) \end{aligned}$$

- **Final value theorem:** $\lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} sF(s)$
- **Initial value theorem:** $f(0^+) = \lim_{s \rightarrow \infty} sF(s)$



Important Laplace Tr. Pairs

	$F(s)$	$f(t)$
■ Impulse function	1	$\delta(t)$
■ Step function	$\frac{1}{s}$	$\mathbf{1}(t)$
■ Exponential decay	$\frac{1}{s+a}$	e^{-at}
■ Sine and cosine	$\frac{\omega}{s^2+\omega^2}$	$\sin(\omega t)$
	$\frac{s}{s^2+\omega^2}$	$\cos(\omega t)$

See Dorf and Bishop, *Table 2.3*, p. 47 and *Table D.1* (App. D) online.



Important Laplace Tr. Pairs

- Damped oscillations

$F(s)$	$f(t)$
$\frac{\omega}{(s+a)^2+\omega^2}$	$e^{-at} \sin(\omega t)$
$\frac{s+a}{(s+a)^2+\omega^2}$	$e^{-at} \cos(\omega t)$
$\frac{\omega_n}{s^2+2\zeta\omega_n s+\omega_n^2}$	$\frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_n \sqrt{1-\zeta^2} t)$

See Dorf and Bishop, *Table 2.3*, p. 47 and *Table D.1* (App. D) online.



Laplace Transforms

- Region of convergence:
 - Where the transform integral converges
 - **The Laplace transform exists only when the integral converges!**
- If $|f(t)| < Me^{at}$ for all positive t , then

$$\int_0^\infty |f(t)|e^{-st} dt < \infty$$
 will converge for $s > a$.

$f(t)$	$F(s)$	R.o.C.
1	$\frac{1}{s}$	$s > 0$
t^n	$\frac{n!}{s^{n+1}}$	$n \in \mathbb{Z} > 0$
t^a	$\frac{\Gamma(a+1)}{s^{a+1}}$	$a > 0$
e^{at}	$\frac{1}{s-a}$	$s > a$
$\cos(at)$	$\frac{s}{s^2+a^2}$	$s > 0$
$e^{at} \sin(bt)$	$\frac{b}{(s-a)^2+b^2}$	$s > a$
$\delta(t-c)$	e^{-cs}	$c > 0$



Example

- Consider the spring-mass-damper system

$$M \frac{d^2 y(t)}{dt^2} + b \frac{dy(t)}{dt} + ky(t) = r(t)$$

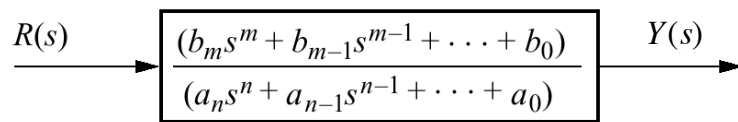
- Assuming the system is **initially at rest** (all initial conditions at zero), then

$$\begin{matrix} \text{output} \leftarrow \\ \text{input} \leftarrow \end{matrix} \boxed{\frac{Y(s)}{R(s)}} = \frac{1}{Ms^2 + bs + k} \leftarrow \text{Transfer function}$$



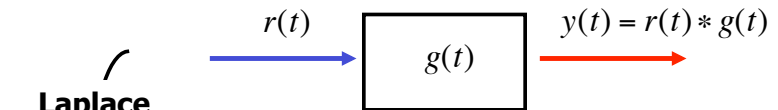
Transfer Function

- Defined as the **ratio** of the Laplace transform of the output to that of the input
- Describes dynamics of a **LTI** system



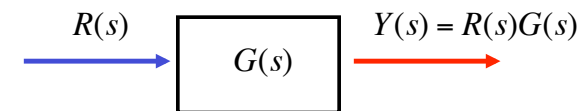
Transfer Function

- Time domain



Laplace transform

- Frequency domain



Transfer Function

- Differential equation replaced by algebraic relation $Y(s)=G(s)R(s)$
- Note that if $R(s)=1$ then $Y(s)=G(s)$ is the **impulse response** of the system
- Note that if $R(s)=1/s$, the unit step function, then $Y(s)=G(s)/s$ is the **step response**
- The magnitude and phase shift of the response to a **sinusoid at frequency ω** is given by the magnitude and phase of the complex number $G(j\omega)$ (see Chapter 8)



Transfer Function

- Using the **Final Value Theorem**, the static or D.C. gain of a transfer function $G(s)$ is given by $G(0)$:

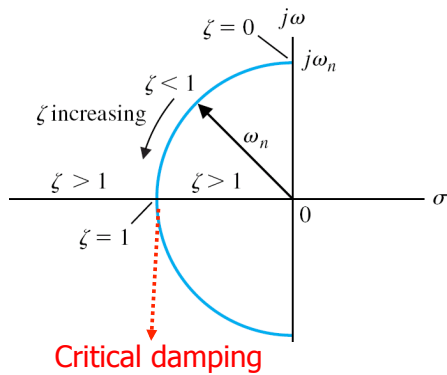
$$\lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} sG(s)$$

- Let $G(s) = N(s)/D(s)$, then
 - Zeros** of $G(s)$ are the roots of $N(s)=0$
 - Poles** of $G(s)$ are the roots of $D(s)=0$



Second Order System Poles **

$$G(s) = \frac{1/M}{s^2 + (b/M)s + (k/M)} = \frac{1/M}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$



Critical damping

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* Damping ratio
 ω_n Natural frequency

In the **underdamped case**
(complex roots due to the quadratic):

$$s_{1,2} = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$

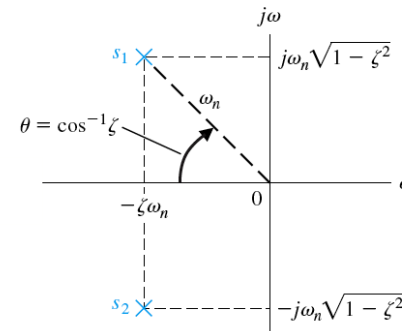
with $\zeta < 1$

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Second Order System Poles **

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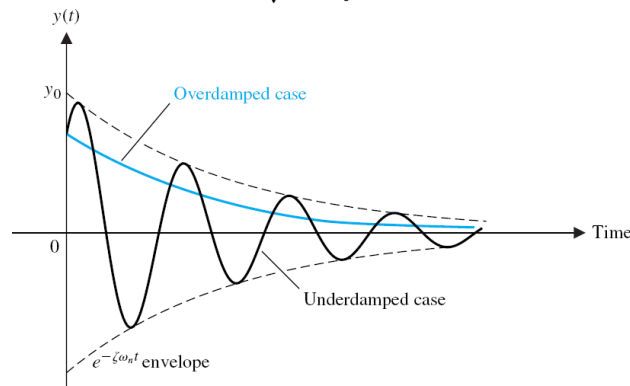
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Natural Response (no input)

$$\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \Leftrightarrow \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_n \sqrt{1-\zeta^2} t), \zeta < 1$$



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Transfer Functions

- A transfer function is
 - **strictly proper** when the degree of the denominator is greater than that of numerator
 - **proper** if those degrees are equal
 - **improper** if the degree of the numerator is greater than that of the denominator

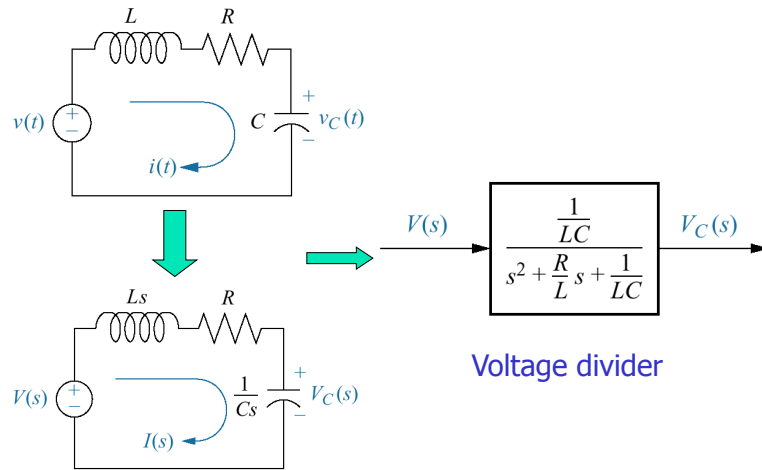
- **Physical systems are proper or strictly proper**

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RLC Network



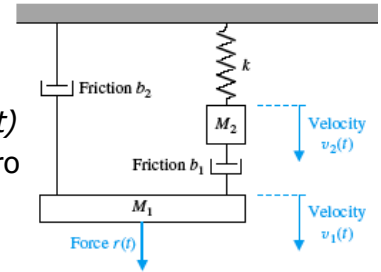
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Example: Spring-mass-damper

- Find transfer function $G(s)$ between the position $x_1(t)$ and the forcing function $r(t)$
- Key assumption: IC are zero
 - $x_1(t)=x_2(t)=0$
 - $dx_1/dx=dx_2/dt=0$
- Note that $x_2(t)$ does not appear explicitly. (Why?)



Dorf and Bishop, Example 2.4, p. 56

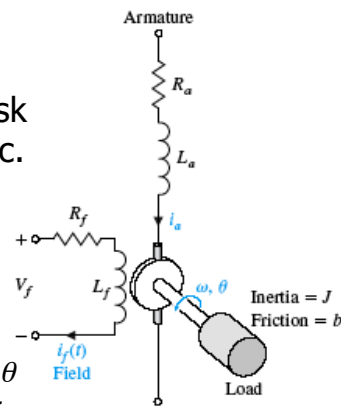
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Example: DC Motor

- Power actuator
- Robotic manipulators, disk drives, machine tools, etc.
- Armature-controlled
 - Input: voltage applied to armature $V_a (=E_a)$
 - Output: angle of rotation θ
 - Control variable: current i_a



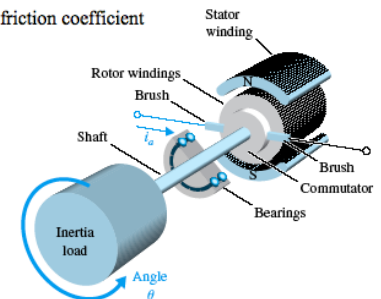
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Example: DC Motor

- | | |
|------------------------------------|--|
| $i_a(t)$ = armature current | L_a = armature inductance |
| R_a = armature resistance | $e_a(t)$ = applied voltage |
| $e_b(t)$ = back emf | K_b = back-emf constant |
| $T_L(t)$ = load torque | ϕ = magnetic flux in the air gap |
| $T_m(t)$ = motor torque | $\omega_m(t)$ = rotor angular velocity |
| $\theta_m(t)$ = rotor displacement | J_m = rotor inertia |
| K_t = torque constant | B_m = viscous friction coefficient |



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Example: DC Motor

- Armature circuit: $e_a(t) - e_b(t) = R_a i_a + L_a \frac{di_a}{dt}$
- Motor relations: $T_m(t) = K_i i_a(t)$
 $e_b(t) = K_b \omega_m(t)$
- Mechanical Response: $J_m \dot{\omega}_m(t) = T_m(t) - T_d(t) - B_m \omega_m(t)$



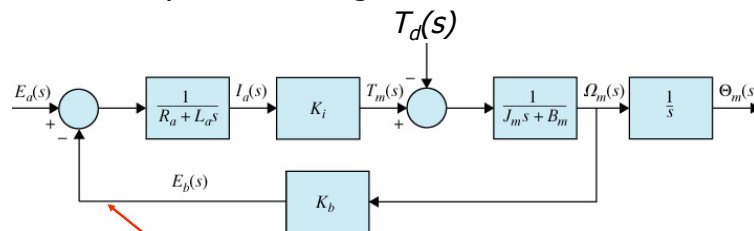
Example: DC Motor

- Armature circuit: $E_a(s) - E_b(s) = (R_a + sL_a)I_a(s)$
- Motor relations: $\begin{cases} T_m(s) = K_i I_a(s) \\ E_b(s) = K_b \Omega_m(s) \end{cases}$
- Mechanical Response: $J_m s \Omega_m(s) = T_m(s) - T_d(s) - B_m \Omega_m(s)$



Example: DC Motor

Using Laplace transform, we can represent this DC motor by the block diagram below



Notice inherent feedback in the model

$$\text{Transfer function : } H(s) = \frac{\theta_m(s)}{E_a(s)}$$



Summary

- **Today**
 - Laplace transform
 - Final Value Theorem
 - Transfer functions
- **Next**
 - Operational Amplifiers
 - Block diagram models