EECE 360 Lecture 14



Feedback Characteristics

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Chapter 5.4, 5.8

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Outline

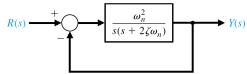
- Review
 - General form of second-order system
 - Natural frequency and critical damping
 - Generic input types
 - Approximations to second-order systems
- Second-order system feedback characteristics
 - Steady-state error
 - Type number

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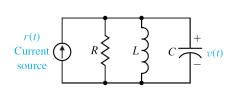


Review: Second-order systems

Transfer function with two poles and no zeros



Examples of 2nd order systems:



x(t) f(t) External Force
Vertical Displacement

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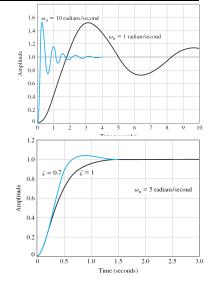


Review: Second-order systems

- Effect of ω_n
 - Frequency of oscillations
- Effect of ζ
 - Damping

$$G(s) = \frac{{\omega_n}^2}{s^2 + 2\zeta\omega_n s + {\omega_n}^2}$$

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Review: Second-order systems

- Underdamped
 - Natural frequency

 $\omega_n > 0$

Damping ratio

 $1 > \zeta > 0$

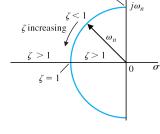
- Critically damped
 - Damping ratio

 $\zeta = 1$

Overdamped

Damping ratio

ζ > 1

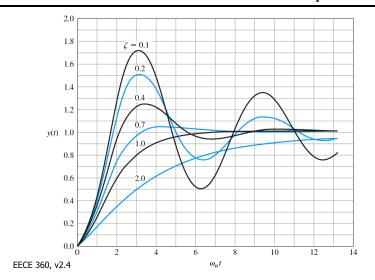


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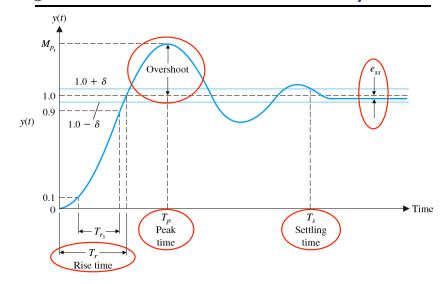


Review: Second-order systems





Review: Second-order systems





Review: Second-order systems

$$T_r \approx \frac{2.16\zeta + 0.60}{\omega_r}$$

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \xi^2}}$$

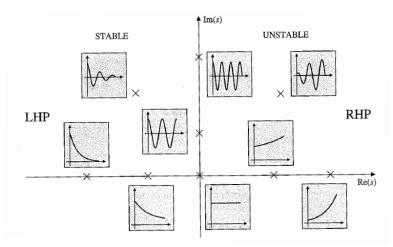
$$M_p = 1 + e^{-\xi \pi / \sqrt{1 - \xi^2}}$$

$$T_s \approx \frac{4}{\xi \omega_n}$$

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s-Domain/Transient Response



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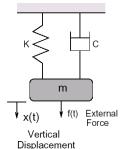


Spring-Mass-Damper System

• Input u=f(t), Output y=x(t)

$$u(t) = m\ddot{x}(t) + b\dot{x}(t) + kx(t)$$

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix} u$$



$$G(s) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s & -1 \\ \frac{k}{m} & s + \frac{b}{m} \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix}$$

$$G(s) = \frac{\frac{1}{m}}{s^2 + \frac{b}{m}s + \frac{k}{m}} = \frac{a\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

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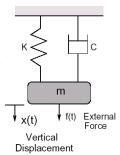


Spring-Mass-Damper System

• Input u=f(t), Output y=x(t)

$$G(s) = \frac{\frac{1}{m}}{s^2 + \frac{b}{m}s + \frac{k}{m}} = \frac{a\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$
$$\omega_n = \sqrt{\frac{k}{m}}, \quad \zeta = \frac{b}{2\sqrt{mk}}, \quad a = m/k$$

- System response
 - Underdamped for $b < 2\sqrt{mk}$
 - Critically damped for $b = 2\sqrt{mk}$
 - Overdamped for $b > 2\sqrt{mk}$



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Spring-Mass-Damper System

 Simulation platform ('Dynamic Systems Demonstrator' at

http://users.ece.gatech.edu/~bonnie/book1/ applets/suspension/MSDdemo.htm

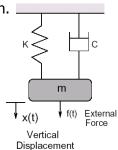
Developed by Prof. Heck, Georgia Tech. I

Exercise:

Pick *b*, *k*, *m* in order to simulate:

- 1) an underdamped response,
- 2) a critically damped response, and
- 3) an overdamped response

with a step input.



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Steady-State Error

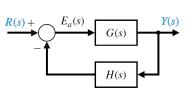
- Reduction or elimination of steady-state error is a fundamental reason for using feedback
- With closed-loop transfer function

$$Y(s) = \frac{G(s)}{1 + G(s)H(s)}R(s)$$

the error

$$E(s) = R(s) - Y(s)$$

$$= \frac{1}{1 + G(s)H(s)}R(s)$$



has steady-state error (with *H(s)*=1)

$$\lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)}$$

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Steady-State Error

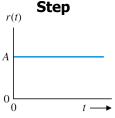
- Steady-state error is another performance metric (e.g. settling time, overshoot, etc.)
- We can classify systems according to their ability to track specific input types.
- This classification is known as a type number. (e.g. a system of type number 0, 1, 2, etc....)
- The type number indicates the number of integrators a system has in G(s).

Question: How many integrators must G(s) contain to be able to exactly track a step? A ramp? A parabola?

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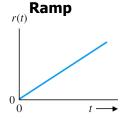


Test Input Signals



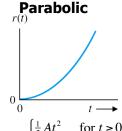
$$r(t) = \begin{cases} A & \text{for } t \ge 0 \\ 0 & \text{otherwise} \end{cases}$$

$$R(s) = \frac{A}{s}$$



$$r(t) = \begin{cases} At & \text{for } t \ge 0 \\ 0 & \text{otherwise} \end{cases}$$

$$R(s) = \frac{A}{c^2}$$



$$r(t) = \begin{cases} \frac{1}{2}At^2 & \text{for } t \ge 0\\ 0 & \text{otherwise} \end{cases}$$

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"Base-case" used to evaluate system response.

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Type Number

- The number of integrators in G(s) indicates its type number
- Step input, R(s) = 1/s:

$$e_{ss} = \lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{s \cdot (1/s)}{1 + G(s)} = \lim_{s \to 0} \frac{1}{1 + G(s)}$$

• Ramp input, $R(s) = 1/s^2$

$$e_{ss} = \lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{s \cdot (1/s^2)}{1 + G(s)} = \lim_{s \to 0} \frac{1}{s + sG(s)} = \lim_{s \to 0} \frac{1}{sG(s)}$$

• Parabolic input, $R(s) = 1/s^3$

$$e_{ss} = \lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{s \cdot (1/s^3)}{1 + G(s)} = \lim_{s \to 0} \frac{1}{s^2 + s^2 G(s)} = \lim_{s \to 0} \frac{1}{s^2 G(s)}$$

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Type Number

Define the constants

$$K_s = \lim_{s \to 0} G(s), \quad K_v = \lim_{s \to 0} sG(s), \quad K_a = \lim_{s \to 0} s^2G(s)$$
 Then the steady-state error for

• Step input, R(s) = 1/s:

$$e_{ss} = \lim_{s \to 0} \frac{1}{1 + G(s)} = \frac{1}{1 + K_s}$$

• Ramp input, $R(s) = 1/s^2$

$$e_{ss} = \lim_{s \to 0} \frac{1}{sG(s)} = \frac{1}{K_v}$$

Parabolic input, R(s) = 1/s³

$$e_{ss} = \lim_{s \to 0} \frac{1}{s^2 G(s)} = \frac{1}{K_a}$$

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Type Number

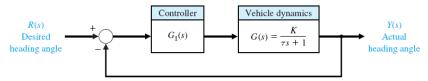
$$K_s = \lim_{s \to 0} G(s), \quad K_v = \lim_{s \to 0} sG(s), \quad K_a = \lim_{s \to 0} s^2G(s)$$

Type Number	Unit Step	Unit Ramp	Unit Parabola
0	$e_{ss} = \frac{1}{1 + K_p}$	Infinite	Infinite
1	$e_{ss} = 0$	$e_{ss} = \frac{1}{K_{v}}$	Infinite
2	$e_{ss} = 0$	$e_{ss} = 0$	$e_{ss} = \frac{1}{K_a}$

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Mobile Steering Robot



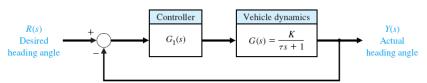
- Case 1: G₁(s)=K₁
 - Open-loop transfer function G₁(s)G(s) is type 0.

$$G_1(s)G(s) = \frac{K_1K}{\tau s + 1}, \quad K_s = \lim_{s \to 0} G_1(s)G(s) = K_1K$$

 Therefore with a step input, the closed-loop system will have steady-state error

$$e_{ss} = \lim_{s \to 0} \frac{1}{1 + G(s)} = \frac{1}{1 + K_s} = \frac{1}{1 + K_1 K}$$

Mobile Steering Robot



• Case 1: G₁(s)=K₂/s

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Open-loop transfer function G₁(s)G(s) is type 1.

$$G_1(s)G(s) = \frac{K_2K}{s(\tau s + 1)}, \quad K_{\nu} = \lim_{s \to 0} sG_1(s)G(s) = K_2K$$

 Therefore with a step input, the closed-loop system will have steady-state error

$$e_{ss} = \lim_{s \to 0} \frac{1}{1 + G_1(s)G(s)} = \lim_{s \to 0} \frac{s(\tau s + 1)}{s(\tau s + 1) + K_2 K} = 0$$

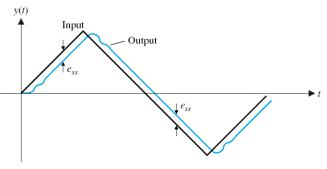
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Mobile Steering Robot

With a ramp input, the steady-state error is

$$e_{ss} = \lim_{s \to 0} \frac{1}{1 + G_1(s)G(s)} = \lim_{s \to 0} \frac{1}{K_v} = \frac{1}{K_2K}$$



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Error for Non-Unity Feedback

- Now consider the case when H(s)≠1
- With error defined as

$$E(s) = R(s) - Y(s)$$

$$= \frac{1 + G(s)H(s) - G(s)}{1 + G(s)H(s)}R(s)$$

$$E_a(s) + E_a(s)$$

$$G(s)$$

$$H(s)$$
the steady-state error is

$$\lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{1 + G(s)H(s) - G(s)}{1 + G(s)H(s)} sR(s)$$

 To find the steady-state error for specific input types, use the same derivation as with unity feedback, but with a different transfer function.

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Example 5.5

The error is

e error is
$$E(s) = R(s) - Y(s)$$

$$= 1 - \frac{K(s+4)}{(s+2)(s+4) + 2K}$$

$$= \frac{(s+2)(s+4-K)}{s^2 + 6s + 8 + 2K}$$

 Therefore with a step input, the closed-loop system will have steady-state error

$$e_{ss} = \lim_{s \to 0} sE(s) \cdot (1/s) = \frac{8 - 2K}{8 + 2K} = \frac{4 - K}{4 + K}$$

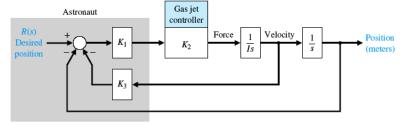
What is the steady-state error with a ramp input?



Example: Astronaut



- Consider an astronaut in space. The astronaut controls position with gas jet propulsion.
- What values of K₁, K₂, K₃ will provide an acceptable system response? The settling time should be 0.3 seconds, the overshoot less than 5%, and steadystate error to a ramp input less than 0.5 m.



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Summary

- Second-order system feedback characteristics
 - Natural frequency, damping ratio
 - Relating poles (s-domain) to transient response
 - Transient response requirements (settling time, overshoot, rise time, peak time)
 - Steady-state error
 - Type number
 - Potential conflicts in designing controllers for multiple transient/steady-state requirements



Next week

- Stability
 - BIBO stability
 - Asymptotic (exponential) stability
 - Conditional stability
 - Relative stability
- Root locus
 - Routh-Hurwitz criterion
 - Root-locus plots
 - Controller design through root-locus

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