



State-space reference tracking and other control problems

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Chapters 11.6-11.8



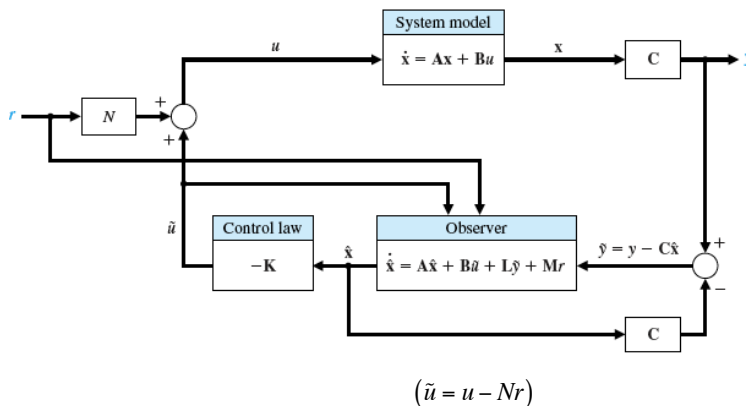
Today's lecture

- LQR Control
 - Choosing closed-loop pole locations through minimization of a cost function
- Static reference tracking
 - Methods for tracking constant-value reference inputs
- Internal Model Control
 - State-space methods for robust tracking of dynamic reference inputs



Reference inputs

- Output-based command following



Reference inputs

- For command following, additional control components may be needed
- The control $u = -Kx + r$ can lead to steady-state errors when tracking a reference input r .
- **Solution:** Pre-multiply r by carefully chosen matrix N

Case 1: Full-state feedback

$$u = -Kx + Nr$$

Case 2: Full-state feedback with full-order observer

$$u = -K\hat{x} + Nr$$

$$\dot{\hat{x}} = A\hat{x} + B(u - Nr) + L(y - C\hat{x}) + Mr$$



Reference inputs: Case 1

Full-state feedback regulation of steady-state output y_{ss} to desired steady-state value r_{ss}

- Standard procedure:

- To track a constant desired position x_{ss} (ss="steady-state") with control u_{ss} note that

$$0 = Ax_{ss} + Bu_{ss}$$

$$y_{ss} = Cx_{ss} + Du_{ss}$$

- and substituting $x_{ss} = N_x r_{ss}$, $u_{ss} = N_u r_{ss}$ we get

$$0 = AN_x r_{ss} + BN_u r_{ss}$$

$$r_{ss} = CN_x r_{ss} + DN_u r_{ss}$$

- when $y_{ss} = r_{ss}$ in the steady-state



Reference inputs: Case 1

- In matrix form,

$$\begin{bmatrix} 0 \\ 1 \end{bmatrix} r_{ss} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} N_x \\ N_u \end{bmatrix} r_{ss}$$

$$\begin{bmatrix} N_x \\ N_u \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

- and therefore the full-state regulating input is

$$u = -Kx + Nr, \quad N = N_u + KN_x$$

$$= -Kx + (N_u + KN_x)r$$

to ensure **no** steady-state error in tracking r .



Reference inputs: Case 2

Command following with full-state feedback and full-order observer

- General form:

$$u = -K\hat{x} + Nr$$

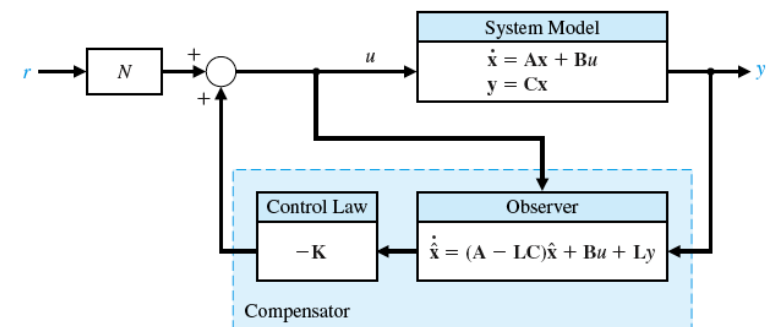
$$\dot{\hat{x}} = A\hat{x} + B(u - Nr) + L(y - C\hat{x}) + Mr$$

- There are a variety of ways to choose M , N
 - Autonomous estimator**: Select M and N so that the state estimator error equation is independent of r
 - Tracking-error estimator**: Select M and N so that only the **tracking** error ($e_r = r - y$) is used in the control
 - And others...



Reference inputs: Case 2

- Autonomous estimator**: Select M and N so that the state estimator error equation is independent of r

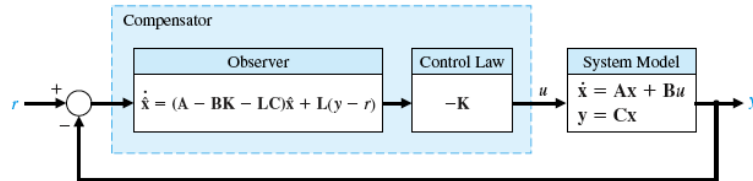




Reference inputs: Case 2

- Tracking-error estimator: Select M and N so that only the **tracking** error ($e_r = r - y$) is used in the control

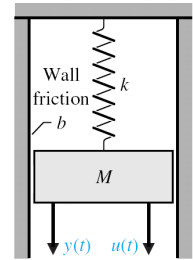
$$N = 0, \quad M = -L$$



Example: Spring-Mass-Damper

- Case 1: No observer

$$\begin{aligned} \begin{bmatrix} N_x \\ N_u \end{bmatrix} &= \begin{bmatrix} A & B \\ C & D \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \\ &= \begin{bmatrix} 0 & 1 & 0 \\ -\frac{k}{M} & -\frac{b}{M} & 1 \\ 1 & 0 & 0 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\ &= \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ \frac{b}{M} & 1 & \frac{k}{M} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ \frac{k}{M} \end{bmatrix} \end{aligned}$$



Example: Spring-Mass-Damper

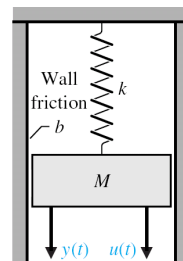
- Case 1: No observer

$$N_x = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad N_u = \frac{k}{M}$$

$$\begin{aligned} u &= -Kx + Nr \\ &= -Kx + \left(N_u + KN_x \right) r \end{aligned}$$

$$= -\left[\omega_n^2 - \frac{k}{M} \quad 2\zeta\omega_n - \frac{b}{M} \right] x + \left[\frac{k}{M} + \left[\omega_n^2 - \frac{k}{M} \quad 2\zeta\omega_n - \frac{b}{M} \right] \begin{bmatrix} 1 \\ 0 \end{bmatrix} \right] r$$

$$= -\left[\omega_n^2 - \frac{k}{M} \quad 2\zeta\omega_n - \frac{b}{M} \right] x + \omega_n^2 r$$

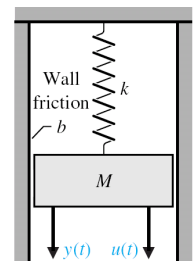


Example: Spring-Mass-Damper

- Case 2: With observer,
- Autonomous estimation (reference input appears in controller but not in estimator)

$$\begin{aligned} N &= \omega_n^2, \quad u = -K\hat{x} + Nr \\ M &= BN = \begin{bmatrix} 0 \\ \omega_n^2 \end{bmatrix} \text{ to make} \\ \dot{e} &= (A - LC)e \end{aligned}$$

- So the estimation dynamics do not depend on the reference command





Example: Spring-Mass-Damper

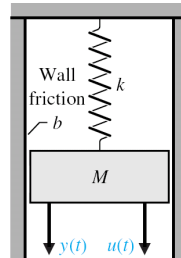
- Case 3: With observer,
- Tracking estimation (reference input r appears in estimator but not in controller)

$$N = 0 \quad u = -K\hat{x}$$

$$M = -L \text{ to make control depend on } \hat{x} \text{ only}$$

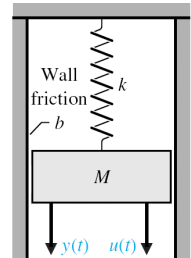
$$\dot{\hat{x}} = (A - BK - LC)\hat{x} + L(y - r)$$

- Comparable to tracking with standard classical control (based on deviations between actual and desired output)



Example: Spring-Mass-Damper

- Because the system is controllable and observable, the closed-loop poles of the error dynamics and the system dynamics can be placed arbitrarily.
- However, the further away the closed-loop poles are placed from the open-loop poles, the higher the control effort.
- Additionally, excessively high observer gains can lead to amplification of noise inherent to the output measurements.



Summary

- Separation principle** allows independent design of the controller and observer
- Generally design controller first, then observer to be faster than the controller
- Reference inputs
 - To track a reference input, the regulating controller/observer must be modified
 - Construct N in $u = -Kx + Nr$ to remove steady-state error with full-state feedback
 - More complicated options in observer design depend on control problem at hand.



Internal Model Principle

- For a step input, **zero steady-state tracking error** can be achieved if the loop transfer function contains one integrator. For a ramp, two, etc...
- This idea can be formalized via the **internal model principle**

Purpose: design a compensator that provides asymptotic tracking of a reference input with **zero steady-state error**.



Internal Model Principle

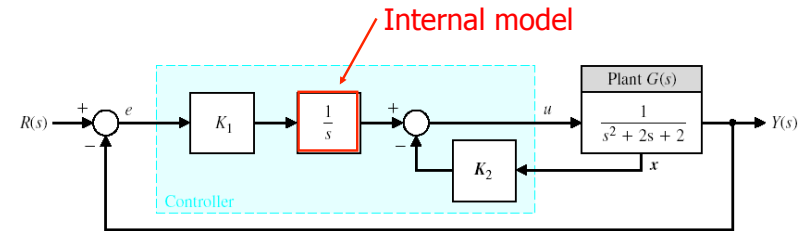
- Consider a unit feedback system with loop transfer function $G(s)G_c(s)$
- The internal model principle states that

If $G(s)G_c(s)$ contains $R(s)$, then $y(t)$ will track $r(t)$ asymptotically.



Internal Model Principle

Example: Internal model design for a step

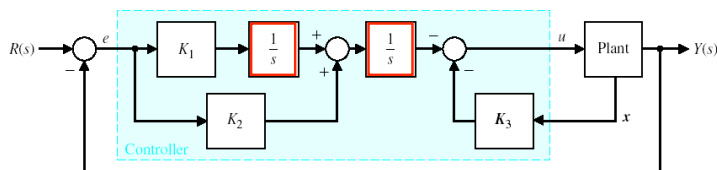


Design of a controller to enable the tracking of a step reference input with zero steady-state error.



Internal Model Principle

Example: Internal model design for a ramp



Can be extended to other types of reference inputs, e.g. sine wave, etc...



Other possibilities

- Kalman filter
 - Observer gain which minimizes effect of noise from measurements
- Linear Quadratic Regulator (LQR)
 - Controller which optimizes a cost function (e.g. minimize fuel usage, error magnitude, control authority, etc.)
- Reduced state-control
 - When only part of x needs to be controlled
- Reduced-order observer
 - When only part of x needs to be estimated
- And **many** others...



Optimal Control

- An alternative to pole placement is **optimal control**.
- We want to find the controller that **minimizes a performance index**



Linear Quadratic Regulator (LQR) Control

- The performance index

$$J = \int_0^{\infty} (x^T Q x + r u^2) dt$$

- is minimized when

$$u(t) = -K^T x \text{ with } K = P B r^{-1}$$

where P satisfies the Riccati equation

$$A^T P + P A - P B B^T P r^{-1} + Q = 0$$



Control Sub-disciplines

- Discrete control
 - Control laws which account for sampling of a continuous signal from a continuous process
- Robust control
 - Design of shaping functions to make the system mathematically robust to uncertainty and noise
- Discrete event systems and control
 - Automata theory for supervisory control
- Optimal control
 - Design and computation of optimal controllers and observers to minimize a specific cost



Control Sub-disciplines

- Nonlinear control
 - Control and observation of general systems $dx/dt=f(x,u)$
- Hybrid control
 - Analysis and design of systems which have continuous processes as well as discrete mode-logic (e.g., hierarchical structure)
- Embedded systems and control
 - Computation and control of systems with integrated physical and computed components
- Biological/biomedical control
 - Analysis and design for biological modeling and biomedical control
- And many others...



Related Disciplines

- Information theory
- Robotics, haptics
- Verification (automata theory)
- Signal processing
- Chemical and industrial processes
- Artificial intelligence, fuzzy logic
- Complex systems, chaos theory
- Dynamics of mechanical systems
- Biological cell signaling and biological networks
- Scientific computation
- Mechatronics, sensors, and actuators