Polyphase Decomposition The Decomposition

• Consider an arbitrary sequence $\{x[n]\}$ with a *z*-transform X(z) given by

$$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$$

• We can rewrite
$$X(z)$$
 as

$$X(z) = \sum_{k=0}^{M-1} z^{-k} X_k(z^M)$$

where

1

$$X_{k}(z) = \sum_{n=-\infty}^{\infty} x_{k}[n] z^{-n} = \sum_{n=-\infty}^{\infty} x[Mn+k] z^{-n}$$
$$0 \le k \le M - 1$$

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- The subsequences {x_k[n]} are called the polyphase components of the parent sequence {x[n]}
- The functions X_k(z), given by the *z*-transforms of {x_k[n]}, are called the polyphase components of X(z)

 The relation between the subsequences {x_k[n]} and the original sequence {x[n]} are given by

$$x_k[n] = x[Mn+k], \quad 0 \le k \le M-1$$

• In matrix form we can write

$$X(z) = \begin{bmatrix} 1 & z^{-1} & \cdots & z^{-(M-1)} \end{bmatrix} \begin{bmatrix} X_0(z^M) \\ X_1(z^M) \\ \vdots \\ X_{M-1}(z^M) \end{bmatrix}$$

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• A multirate structural interpretation of the polyphase decomposition is given below



- The polyphase decomposition of an FIR transfer function can be carried out by inspection
- For example, consider a length-9 FIR transfer function:

$$H(z) = \sum_{n=0}^{8} h[n] z^{-n}$$

• Its 4-branch polyphase decomposition is given by $H(z) = E_0(z^4) + z^{-1}E_1(z^4) + z^{-2}E_2(z^4) + z^{-3}E_3(z^4)$

where

$$E_0(z) = h[0] + h[4]z^{-1} + h[8]z^{-2}$$

 $E_1(z) = h[1] + h[5]z^{-1}$
 $E_2(z) = h[2] + h[6]z^{-1}$
 $E_3(z) = h[3] + h[7]z^{-1}$



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- The polyphase decomposition of an IIR transfer function H(z) = P(z)/D(z) is not that straight forward
- One way to arrive at an *M*-branch polyphase decomposition of *H*(*z*) is to express it in the form *P*'(*z*)/*D*'(*z*^{*M*}) by multiplying *P*(*z*) and *D*(*z*) with an appropriately chosen polynomial and then apply an *M*-branch polyphase decomposition to *P*'(*z*)

• <u>Example</u> - Consider

$$H(z) = \frac{1 - 2z^{-1}}{1 + 3z^{-1}}$$

- To obtain a 2-band polyphase decomposition we rewrite H(z) as $H(z) = \frac{(1-2z^{-1})(1-3z^{-1})}{(1+3z^{-1})(1-3z^{-1})} = \frac{1-5z^{-1}+6z^{-2}}{1-9z^{-2}} = \frac{1+6z^{-2}}{1-9z^{-2}} + \frac{-5z^{-1}}{1-9z^{-2}}$
 - Therefore,

$$H(z) = E_0(z^2) + z^{-1}E_1(z^2)$$

where $E_0(z) = \frac{1+6z^{-1}}{1-9z^{-1}}, \quad E_1(z) = \frac{-5}{1-9z^{-1}}$

- Note: The above approach increases the overall order and complexity of *H*(*z*)
- However, when used in certain multirate structures, the approach may result in a more computationally efficient structure
- An alternative more attractive approach is discussed in the following example

• Example - Consider the transfer function of a 5-th order Butterworth lowpass filter with a 3-dB cutoff frequency at 0.5π : $0.0527864(1+z^{-1})^5$

 $H(z) = \frac{0.0527864(1+z^{-1})^5}{1+0.633436854z^{-2}+0.0557281z^{-2}}$

• It is easy to show that H(z) can be expressed as $H(z) = \frac{1}{2} \left[\left(\frac{0.105573 + z^{-2}}{1 + 0.105573 z^{-2}} \right) + z^{-1} \left(\frac{0.52786 + z^{-2}}{1 + 0.52786 z^{-2}} \right) \right]$

• Therefore H(z) can be expressed as $H(z) = E_0(z^2) + z^{-1}E_1(z^2)$

where

$$E_0(z) = \frac{1}{2} \left(\frac{0.105573 + z^{-1}}{1 + 0.105573 z^{-1}} \right)$$
$$E_1(z) = \frac{1}{2} \left(\frac{0.52786 + z^{-1}}{1 + 0.52786 z^{-1}} \right)$$

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- Note: In the above polyphase decomposition, branch transfer functions E_i(z) are stable allpass functions
- Moreover, the decomposition has not increased the order of the overall transfer function *H*(*z*)

FIR Filter Structures Based on Polyphase Decomposition

- We shall demonstrate later that a parallel realization of an FIR transfer function *H*(*z*) based on the polyphase decomposition can often result in computationally efficient multirate structures
- Consider the *M*-branch Type I polyphase decomposition of *H*(*z*):

$$H(z) = \sum_{k=0}^{M-1} z^{-k} E_k(z^M)$$

FIR Filter Structures Based on Polyphase Decomposition

• A direct realization of *H*(*z*) based on the Type I polyphase decomposition is shown below



FIR Filter Structures Based on Polyphase Decomposition

• The transpose of the Type I polyphase FIR filter structure is indicated below



FIR Filter Structures Based on Polyphase Decomposition

- An alternative representation of the transpose structure shown on the previous slide is obtained using the notation $R_{\ell}(z^{M}) = E_{M-1-\ell}(z^{M}), \quad 0 \le \ell \le M-1$
- Substituting the above notation in the Type I polyphase decomposition we arrive at the Type II polyphase decomposition:

$$H(z) = \sum_{\ell=0}^{M-1} z^{-(M-1-\ell)} R_{\ell}(z^{M})$$

FIR Filter Structures Based on Polyphase Decomposition

• A direct realization of H(z) based on the Type II polyphase decomposition is shown below



• Consider first the single-stage factor-of-*M* decimator structure shown below

$$x[n] \rightarrow H(z) \xrightarrow{v[n]} M \rightarrow y[n]$$

• We realize the lowpass filter *H*(*z*) using the Type I polyphase structure as shown on the next slide

• Using the cascade equivalence #1 we arrive at the computationally efficient decimator structure shown below on the right



Decimator structure based on Type I polyphase decomposition

- To illustrate the computational efficiency of the modified decimator structure, assume *H*(*z*) to be a length-*N* structure and the input sampling period to be *T* = 1
- Now the decimator output y[n] in the original structure is obtained by down-sampling the filter output v[n] by a factor of *M*

- It is thus necessary to compute v[n] at n = ..., -2M, -M, 0, M, 2M, ...
- Computational requirements are therefore N multiplications and (N-1) additions per output sample being computed
- However, as *n* increases, stored signals in the delay registers change

- Hence, all computations need to be completed in one sampling period, and for the following (M - 1) sampling periods the arithmetic units remain idle
- The modified decimator structure also requires *N* multiplications and (*N*−1) additions per output sample being computed

- However, here the arithmetic units are operative at all instants of the output sampling period which is *M* times that of the input sampling period
- Similar savings are also obtained in the case of the interpolator structure developed using the polyphase decomposition

Computationally Efficient Interpolators

• Figures below show the computationally efficient interpolator structures



Interpolator based on Type I polyphase decomposition



Interpolator based on Type II polyphase decomposition

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- More efficient interpolator and decimator structures can be realized by exploiting the symmetry of filter coefficients in the case of linear-phase filters *H*(*z*)
- Consider for example the realization of a factor-of-3 (*M* = 3) decimator using a length-12 Type 1 linear-phase FIR lowpass filter

- The corresponding transfer function is $H(z) = h[0] + h[1]z^{-1} + h[2]z^{-2} + h[3]z^{-3} + h[4]z^{-4} + h[5]z^{-5} + h[5]z^{-6} + h[4]z^{-7} + h[3]z^{-8} + h[2]z^{-9} + h[1]z^{-10} + h[0]z^{-11}$
 - A conventional polyphase decomposition of H(z) yields the following subfilters: $E_0(z) = h[0] + h[3]z^{-1} + h[5]z^{-2} + h[2]z^{-3}$ $E_1(z) = h[1] + h[4]z^{-1} + h[4]z^{-2} + h[1]z^{-3}$ $E_2(z) = h[2] + h[5]z^{-1} + h[3]z^{-2} + h[0]z^{-3}$

- Note that $E_1(z)$ still has a symmetric impulse response, whereas $E_0(z)$ is the mirror image of $E_2(z)$
- These relations can be made use of in developing a computationally efficient realization using only 6 multipliers and 11 two-input adders as shown on the next slide

• Factor-of-3 decimator with a linear-phase decimation filter



A Useful Identity

• The cascade multirate structure shown below appears in a number of applications

$$x[n] \longrightarrow \uparrow L \longrightarrow H(z) \longrightarrow \downarrow L \longrightarrow y[n]$$

• Equivalent time-invariant digital filter obtained by expressing H(z) in its *L*-term Type I polyphase form $\sum_{k=0}^{L-1} z^{-k} E_k(z^L)$ is shown below $x[n] \longrightarrow E_0(z) \longrightarrow y[n]$

Arbitrary-Rate Sampling Rate Converter

- The estimation of a discrete-time signal value at an arbitrary time instant between a consecutive pair of known samples can be solved by using some type of interpolation
- In this approach an approximating continuous-time signal is formed from a set of known consecutive samples of the given discrete-time signal

Arbitrary-Rate Sampling Rate Converter

- The value of the approximating continuoustime signal is then evaluated at the desired time instant
- This interpolation process can be directly implemented by designing a digital interpolation filter

$$x[n] \xrightarrow{x_a(t)} G_a(s) \xrightarrow{x_a(t)} f_T = \frac{1}{T}$$

$$F_T = \frac{1}{T}$$

$$F_T = \frac{1}{T}$$

- In principle, a sampling rate conversion by an arbitrary conversion factor can be implemented as follows
- The input digital signal is passed through an ideal analog reconstruction lowpass filter whose output is resampled at the desired output rate as indicated below

$$x[n] \xrightarrow{\hat{x}_a(t)} G_a(s) \xrightarrow{\hat{x}_a(t)} F_T = \frac{1}{T}$$

$$F_T = \frac{1}{T}$$

$$F_T = \frac{1}{T}$$

- Let the impulse response of the analog lowpass filter is denoted by $g_a(t)$
- Then the output of the filter is given by $\hat{x}_a(t) = \sum_{\ell=-\infty}^{\infty} x[\ell] g_a(t - \ell T)$
- If the analog filter is chosen to bandlimit its output to the frequency range $F_g < F_T'/2$, its output $\hat{x}_a(t)$ can then be resampled at the rate F_T'

- Since the impulse response g_a(t) of an ideal lowpass analog filter is of infinite duration and the samples g_a(nT'-ℓT) have to be computed at each sampling instant, implementation of the ideal bandlimited interpolation algorithm in exact form is not practical
- Thus, an approximation is employed in practice

- Problem statement: Given $N_2 + N_1 + 1$ input signal samples, x[k], $k = -N_1, ..., N_2$, obtained by sampling an analog signal $x_a(t)$ at $t = t_k$ $= t_0 + kT_{in}$, determine the sample value $x_a(t_0 + kT_{in}) = y[\alpha]$ at time instant $t' = t_0 + kT_{in}$ where $-N_1 \le \alpha \le N_2$
- Figure on the next slide illustrates the interpolation process by an arbitrary factor



• We describe next a commonly employed interpolation algorithm based on a finite weighted sum of input samples

• Here, a polynomial approximation $\hat{x}_a(t)$ to $x_a(t)$ is defined as

$$\hat{x}_{a}(t) = \sum_{k=-N_{1}}^{N_{2}} P_{k}(t) x[n+k]$$

where $P_k(t)$ are the Lagrange polynomials given by

$$P_{k}(t) = \prod_{\substack{\ell = -N_{1} \\ \ell \neq k}}^{N_{2}} \left(\frac{t - t_{k}}{t_{k} - t_{\ell}} \right), \quad -N_{1} \leq k \leq N_{2}$$

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- <u>Example</u> Design a fractional-rate interpolator with an interpolation factor of 3/2 using a 3rd-order polynomial approximation with $N_1 = 2$ and $N_2 = 1$
- The output *y*[*n*] of the interpolator is thus computed using

$$y[n] = P_{-2}(\alpha)x[n-2] + P_{-1}(\alpha)x[n-1] + P_0(\alpha)x[n] + P_1(\alpha)x[n+1]$$

• Here, the Lagrange polynomials are given by

$$P_{-2}(\alpha) = \frac{(\alpha+1)\alpha(\alpha-1)}{-6} = \frac{1}{6}(-\alpha^3 + \alpha)$$

$$P_{-1}(\alpha) = \frac{(\alpha+2)\alpha(\alpha-1)}{2} = \frac{1}{2}(\alpha^3 + \alpha^2 - 2\alpha)$$

$$P_{0}(\alpha) = \frac{(\alpha+2)(\alpha+1)(\alpha-1)}{-2} = -\frac{1}{2}(\alpha^3 + 2\alpha^2 - \alpha - 2)$$

$$P_{1}(\alpha) = \frac{(\alpha+2)(\alpha+1)\alpha}{-6} = \frac{1}{6}(\alpha^3 + 3\alpha^2 + \alpha)$$

- Figure below shows the locations of the samples of the input and the output for an interpolator with a conversion factor of 3/2
- Locations of the output samples y[0], y[1], and y[2] in the input sample domain are marked with an arrow



Input sample index Output sample index

- From the figure on the previous slide it can be seen that the value of α for computation of y[n], to be labeled α₀, is 0
- Substituting this value of α in the expressions for the Lagrange polynomial coefficients derived earlier we get $P_{-2}(\alpha_0) = 0$, $P_{-1}(\alpha_0) = 0$

$$P_0(\alpha_0) = 1$$
, $P_1(\alpha_0) = 0$

- The value of α for computation of y[n+1], to be labeled α₁, is 2/3
- Substituting this value of α in the expressions for the Lagrange polynomial coefficients we get

$$P_{-2}(\alpha_1) = 0.0617$$
, $P_{-1}(\alpha_1) = -0.2963$
 $P_0(\alpha_1) = 0.7407$, $P_1(\alpha_1) = 0.4938$

- The value of α for computation of y[n+2], to be labeled α₂, is 4/3
- Substituting this value of α in the expressions for the Lagrange polynomial coefficients we get

$$\begin{split} P_{-2}(\alpha_2) &= -0.1728 , \ P_{-1}(\alpha_2) = 0.7407 \\ P_0(\alpha_2) &= -1.2963 , \ P_1(\alpha_2) = 1.7284 \end{split}$$

• Substituting the values of the Lagrange polynomial coefficients in the interpolator output equation for *n*, *n*+1, and *n*+2, and combining the three equations into a matrix form we arrive at

$$\begin{bmatrix} y[n] \\ y[n+1] \\ y[n+2] \end{bmatrix} = \begin{bmatrix} P_{-2}(\alpha_0) & P_{-1}(\alpha_0) & P_0(\alpha_0) & P_1(\alpha_0) \\ P_{-2}(\alpha_1) & P_{-1}(\alpha_1) & P_0(\alpha_1) & P_1(\alpha_1) \\ P_{-2}(\alpha_2) & P_{-1}(\alpha_2) & P_0(\alpha_2) & P_1(\alpha_2) \end{bmatrix} \begin{vmatrix} x[n-2] \\ x[n-1] \\ x[n] \\ x[n] \\ x[n+1] \end{vmatrix}$$

• The input-output relation of the interpolation filter can be compactly written as $\sum x[n-21]$

$$\begin{bmatrix} y[n]\\y[n+1]\\y[n+2] \end{bmatrix} = \mathbf{H} \begin{bmatrix} x[n-2]\\x[n-1]\\x[n]\\x[n]\\x[n+1] \end{bmatrix}$$

where **H** is the block coefficient matrix

• For the factor-of-3/2 interpolator, we have

	0	0	1	0
$\mathbf{H} =$	0.0617	-0.2963	0.7407	0.4938
	-0.1728	0.7407	-1.2963	1.7284

• It should be evident from an examination of

that the filter coefficients to compute y[n+3], y[n+4], and y[n+5] are again given by the same block matrix **H**

- The desired interpolation filter is a time-varying filter
- A realization of the interpolator is given below



- Note: In practice, the overall system delay will be 3 sample periods
- Hence, the output sample *y*[*n*] actually will appear at the time index *n*+3
- A realization of the factor-of-3 interpolator in the form of a time-varying filter is shown on the next slide



• The coefficients of the 5-th order timevarying FIR filter have a period of 3 and are assigned the values indicated below

Time	$h_0[n]$	$h_1[n]$	$h_2[n]$	$h_3[n]$	$h_4[n]$	$h_5[n]$
3ℓ $3\ell+1$ $3\ell+2$	$ \begin{array}{c} P_1(\alpha_0) \\ 0 \\ 0 \end{array} $	$P_0(\alpha_0)$ $P_1(\alpha_1)$ 0	$P_{-1}(\alpha_0)$ $P_0(\alpha_1)$ $P_1(\alpha_2)$	$\begin{array}{l} P_{-2}(\alpha_{0}) \\ P_{-1}(\alpha_{1}) \\ P_{0}(\alpha_{2}) \end{array}$	0 $P_{-2}(\alpha_1)$ $P_{-1}(\alpha_2)$	0 0 $P_{-2}(\alpha_2)$

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• Substituting the expressions for the Lagrange polynomials in the output equation we arrive at

$$y[n] = \alpha^{3}(-\frac{1}{6}x[n-2] + \frac{1}{2}x[n-1] - \frac{1}{2}x[n] + \frac{1}{6}x[n+1])$$

+ $\alpha^{2}(\frac{1}{2}x[n-1] - x[n] + \frac{1}{2}x[n+1])$
+ $\alpha(\frac{1}{6}x[n-2] - x[n-1] + \frac{1}{2}x[n] + \frac{1}{3}x[n+1])$
+ $x[n]$

• A digital filter realization of the equation on the previous slide leads to the Farrow structure shown below



• In the above structure

$$H_0(z) = -\frac{1}{6}z^{-2} + \frac{1}{2}z^{-1} - \frac{1}{2} + \frac{1}{6}z$$
$$H_1(z) = \frac{1}{2}z^{-1} - 1 + \frac{1}{2}z$$
$$H_2(z) = \frac{1}{6}z^{-2} - z^{-1} + \frac{1}{2} + \frac{1}{3}z$$

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- In the Farrow structure only the value of a is changed periodically with the remaining digital filter structure kept unchanged
- Figures on the next slide show the input and the output of the above interpolator for a sinusoidal input of frequency of 0.05 Hz sampled at a 1-Hz rate



Arbitrary-Rate Sampling Rate Converter

Practical Considerations

- A direct design of a fractional-rate sampling rate converter in most applications is not practical
- This is due to two main reasons:
 - length of the time-varying filter needed is usually very large
 - real-time computation of the corresponding filter coefficients is nearly impossible

Arbitrary-Rate Sampling Rate Converter

• As a result, the fractional-rate sampling rate converter is almost realized in a hybrid form as indicated below for the case of an interpolator



• The digital sampling rate converter can be implemented in a multistage form to reduce the computational complexity