THEVENIN'S AND NORTON'S THEOREMS

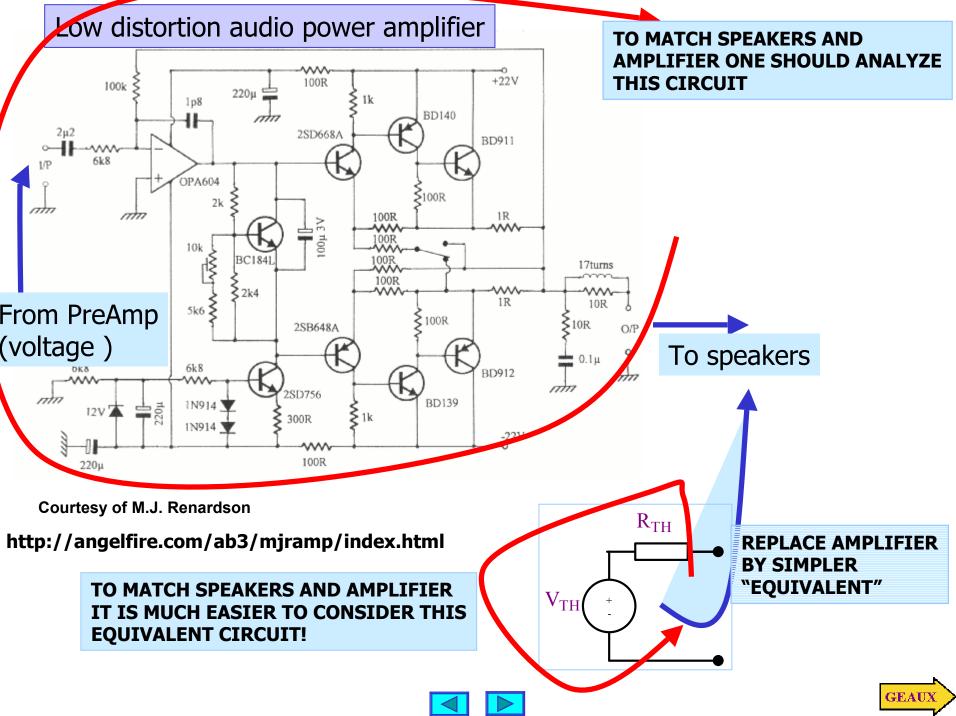
These are some of the most powerful analysis results to be discussed.

They permit to hide information that is not relevant and concentrate in what is important to the analysis



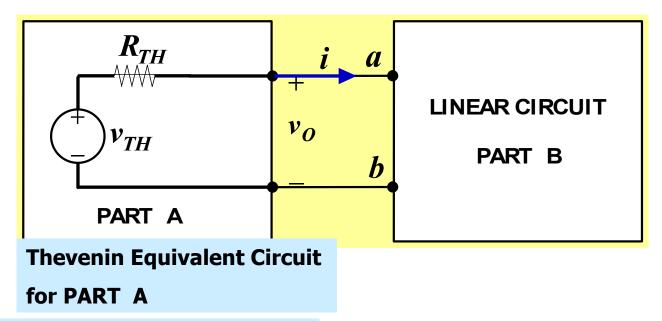






THEVENIN'S EQUIVALENCE THEOREM

LINEAR CIRCUIT LINEAR CIRCUIT a May contain May contain independent and independent and v_o dependent sources dependent sources with their controlling with their controlling variables variables PART A PART B



 v_{TH} Thevenin Equivalent Source R_{TH} Thevenin Equivalent Resistance

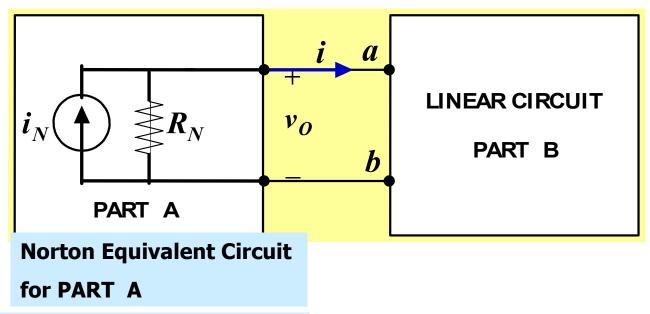






NORTON'S EQUIVALENCE THEOREM

LINEAR CIRCUIT LINEAR CIRCUIT a May contain May contain independent and independent and v_o dependent sources dependent sources with their controlling with their controlling variables variables PART A PART B



 i_N Thevenin Equivalent Source

 R_N

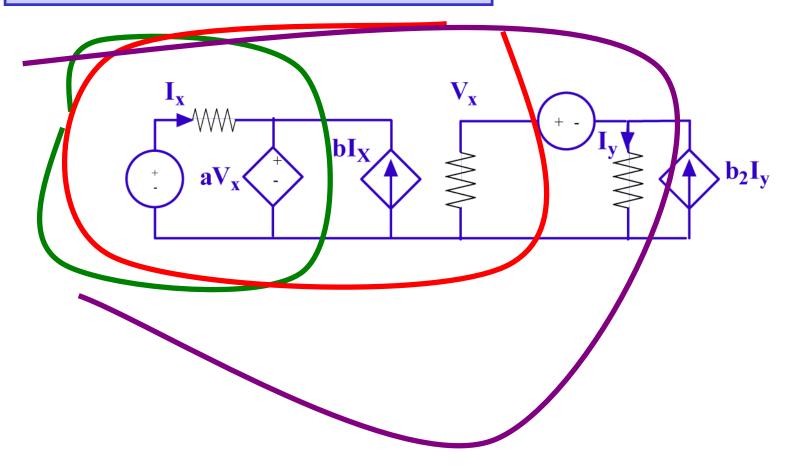
Thevenin Equivalent Resistance







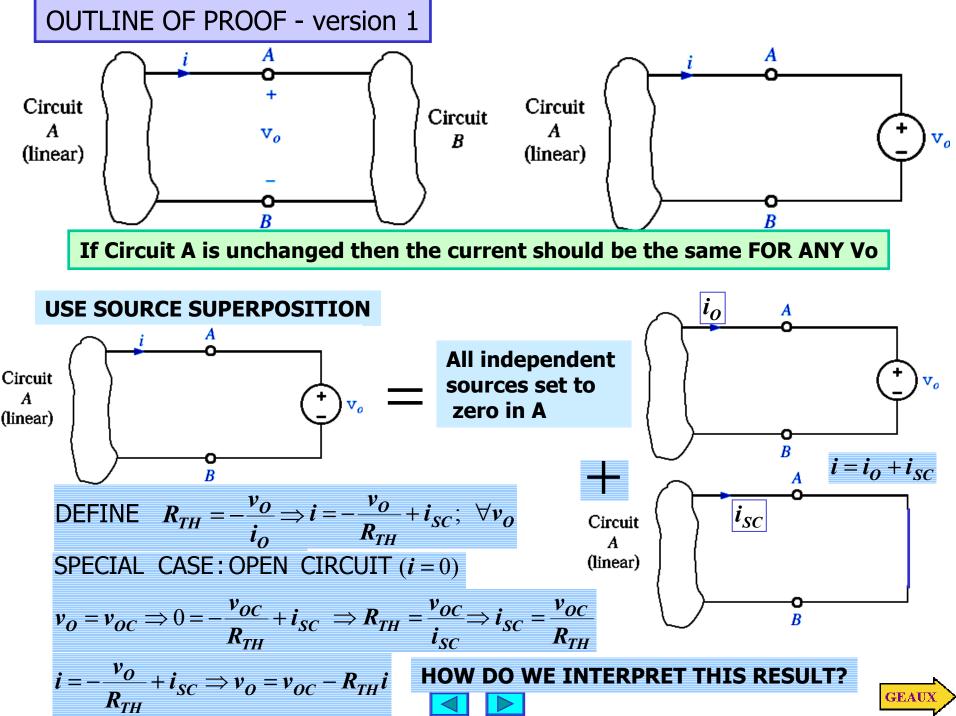
Examples of Valid and Invalid Partitions



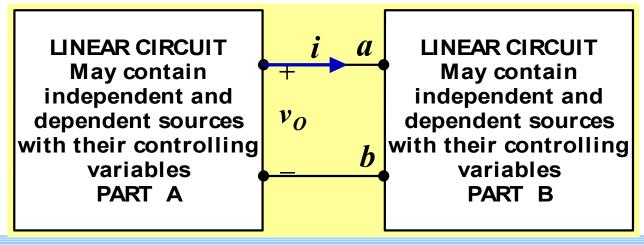








OUTLINE OF PROOF - version 2



- 1. Because of the linearity of the models, for any Part B the relationship between Vo and the current, i, has to be of the form $v_O = m * i + n$
- 2. Result must hold for "every valid Part B" that we can imagine
- 3. If part B is an open circuit then i=0 and... $n = v_{OC}$
- 4. If Part B is a short circuit then Vo is zero. In this case

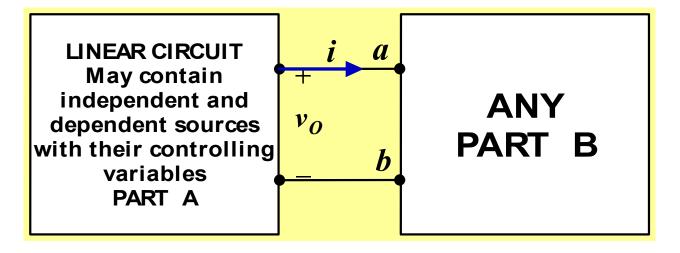
$$0=m^*i_{SC}+v_{OC} \Rightarrow m=-\frac{v_{OC}}{i_{SC}}=-R_{TH}$$

$$v_O = -R_{TH}i + v_{OC}$$

How do we interpret this?

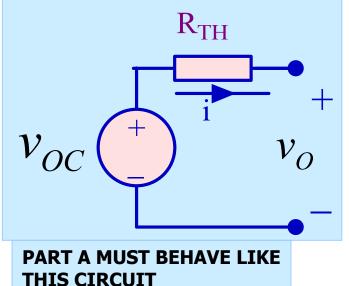


THEVENIN APPROACH



$$v_O = -R_{TH}i + v_{OC}$$

For ANY circuit in Part B



This is the Thevenin equivalent circuit for the circuit in Part A

The voltage source is called the THEVENIN EQUIVALENT SOURCE

The resistance is called the THEVENIN EQUIVALENT RESISTANCE



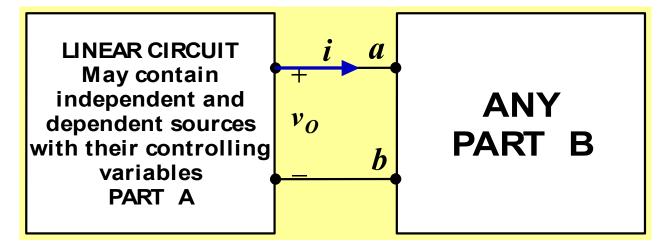


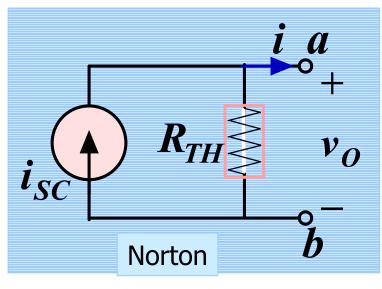


Norton Approach

$$v_O = v_{OC} - R_{TH}i \Rightarrow i = \frac{v_{OC}}{R_{TH}} - \frac{v_O}{R_{TH}}$$

$$\frac{v_{OC}}{R_{TH}} = i_{SC}$$





Norton Equivalent Representation for Part A

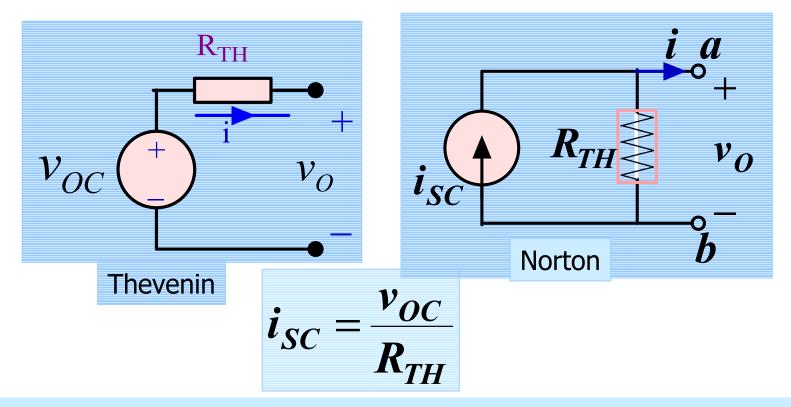
i_{SC} Norton Equivalent Source







ANOTHER VIEW OF THEVENIN'S AND NORTON'S THEOREMS



This equivalence can be viewed as a source transformation problem It shows how to convert a voltage source in series with a resistor into an equivalent current source in parallel with the resistor

SOURCE TRANSFORMATION CAN BE A GOOD TOOL TO REDUCE THE COMPLEXITY OF A CIRCUIT





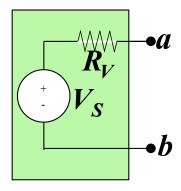


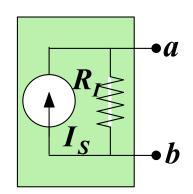
Source transformation is a good tool to reduce complexity in a circuit ...

WHEN IT CAN BE APPLIED!!

"ideal sources" are not good models for real behavior of sources

A real battery does not produce infinite current when short-circuited





THE MODELS ARE EQUIVALENTS WHEN

$$R_V = R_I = R$$
 $V_S = RI_S$

$$V_S = RI_S$$

Improved model Improved model for voltage source for current source

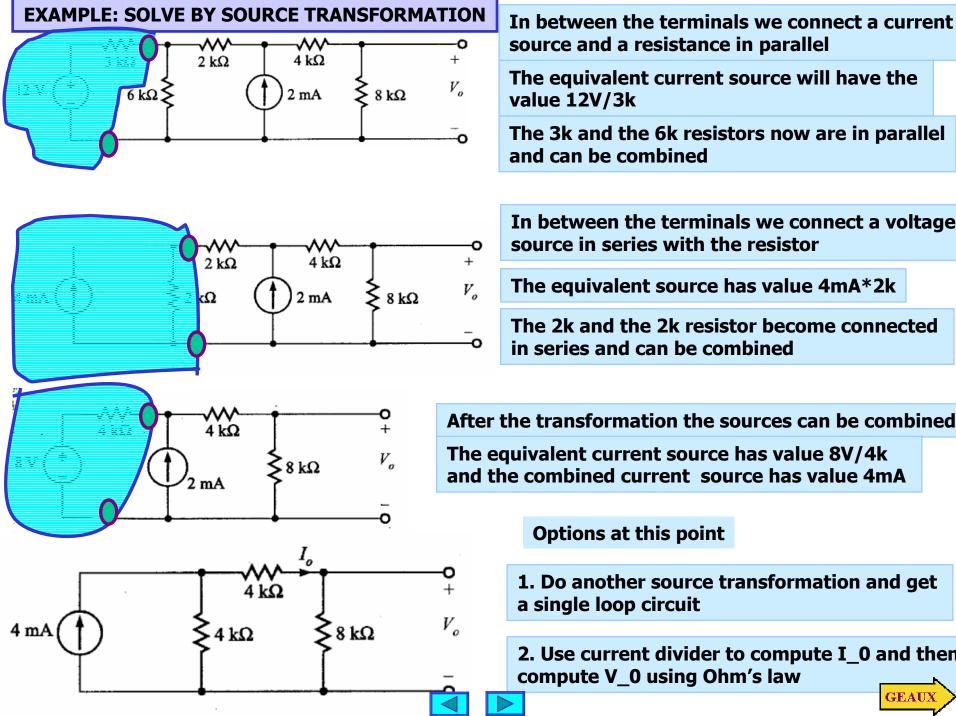
Source Transformationcan be used to determine the Thevenin or Norton Equivalent...

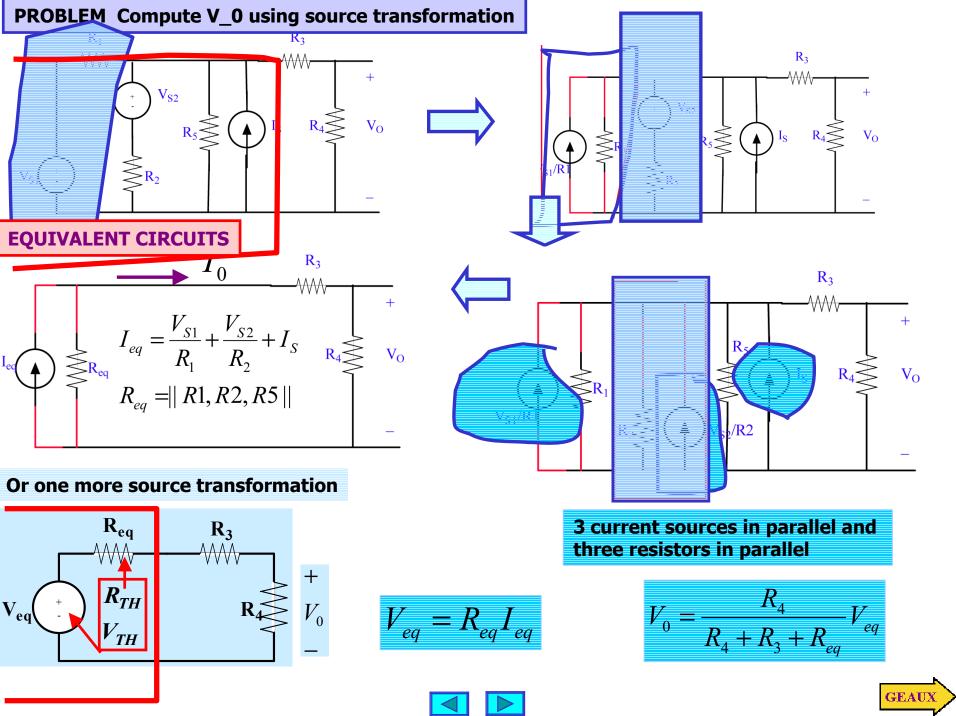
BUT THERE MAY BE MORE EFFICIENT TECHNIQUES



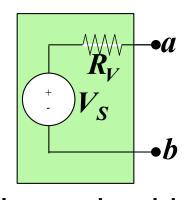


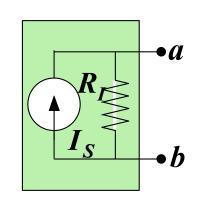






RECAP OF SOURCE TRANSFORMATION





THE MODELS ARE EQUIVALENTS WHEN

$$R_V = R_I = R$$

$$V_S = RI_S$$

Improved model for voltage source for current source

Improved model

Source Transformationcan be used to determine the Thevenin or Norton Equivalent...

WE NOW REVIEW SEVERAL EFFICIENT APPROACHES TO DETERMINE THEVENIN OR NORTON EQUIVALENT **CIRCUITS**







A General Procedure to Determine the Thevenin Equivalent

 v_{TH} Open Circuit voltage voltage at a - b if Part B is removed i_{SC} Short Circuit Current current through a - b if Part B is replaced by a short circuit

$$R_{TH} = \frac{v_{TH}}{i_{SC}}$$
 Thevenin Equivalent Resistance

1. Determine the Thevenin equivalent source

Remove part B and compute the OPEN CIRCUIT voltage V_{ab}

2. Determine the SHORT CIRCUIT current

Remove part B and compute the SHORT CIRCUIT current I_{ab}

$$v_{TH} = v_{OC}, R_{TH} = \frac{v_{OC}}{i_{SC}}$$





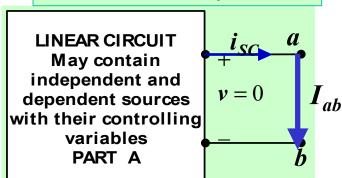
One circuit problem

voc

LINEAR CIRCUIT

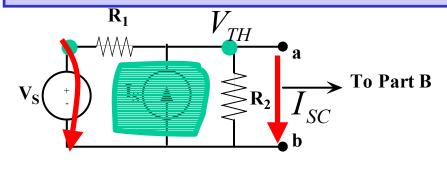
May contain
independent and
dependent sources
with their controlling
variables
PART A

Second circuit problem





AN EXAMPLE OF DETERMINING THE THEVENIN EQUIVALENT



Now for the short circuit current Lets try source superposition

When the current source is open the current through the short circuit is $I_{SC}^1 = \frac{V_S}{R}$

When the voltage source is set to zero, the current through the short circuit is
$$I_{SC}^{\,2}=I_S$$

$$I_{SC} = I_S + \frac{V_S}{R_1}$$

To compute the Thevenin resistance we use

$$R_{TH} = \frac{V_T}{I_S}$$

For this case the Thevenin resistance can be computed as the resistance from a - b when all independent sources have been set to zero

Part B is irrelevant.

The voltage V_ab will be the value of the Thevenin equivalent source.

What is an efficient technique to compute the open circuit voltage?

$$\begin{split} &\frac{V_{TH}}{R_2} + \frac{V_{TH} - V_S}{R_1} - I_S = 0\\ &(\frac{1}{R_1} + \frac{1}{R_2})V_{TH} = \frac{V_S}{R_1} + I_S\\ &V_{TH} = \frac{R_2}{R_1 + R_2}V_S + \frac{R_1R_2}{R_1 + R_2}I_S \end{split}$$

$$V_{TH} = \frac{R_1 R_2}{R_1 + R_2} \left(\frac{V_S}{R_1} + I_S \right)$$

 $R_{TH} = \frac{R_1 R_2}{R_1 + R_2}$

Is this a general

NODE

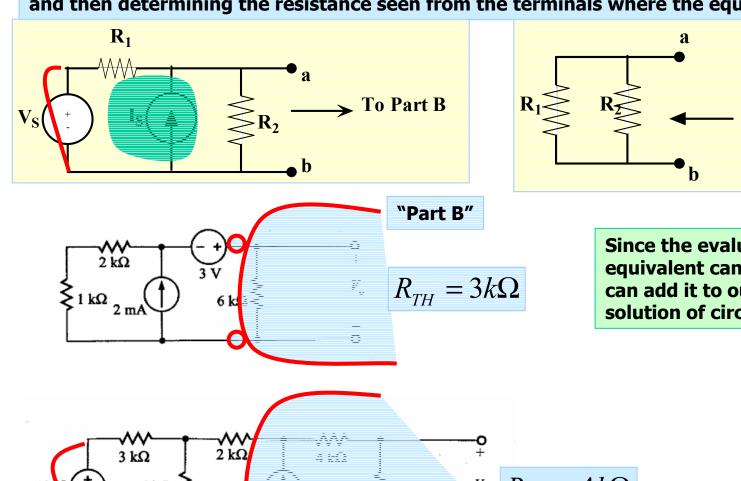
ANALYSIS

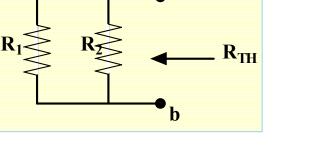
result?

Determining the Thevenin Equivalent in Circuits with Only INDEPENDENT SOURCES

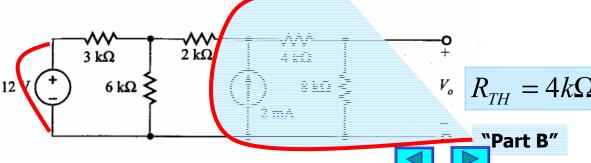
The Thevenin Equivalent Source is computed as the open loop voltage

The Thevenin Equivalent Resistance CAN BE COMPUTED by setting to zero all the sources and then determining the resistance seen from the terminals where the equivalent will be placed





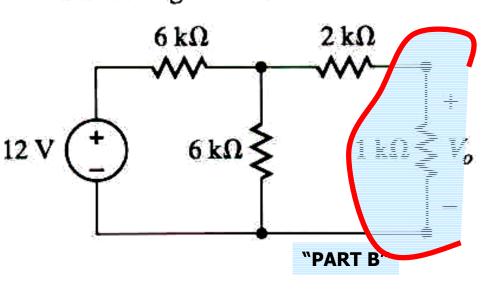
Since the evaluation of the Thevenin equivalent can be very simple, we can add it to our toolkit for the solution of circuits!!

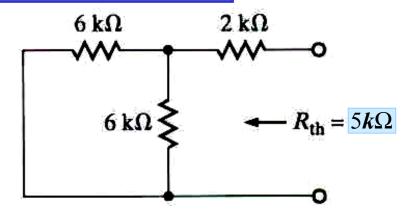


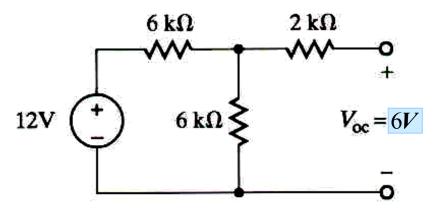


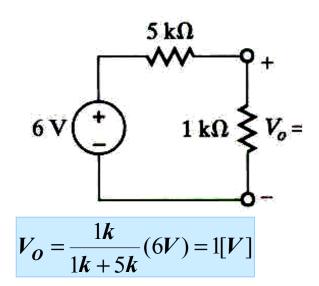
Find V_o in the following network using Thévenin's theorem.

LEARNING BY DOING









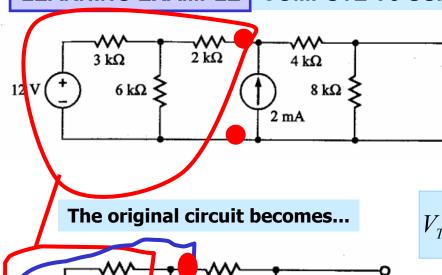






LEARNING EXAMPLE | COMPUTE Vo USING THEVENIN

 $8 k\Omega$



 $4 k\Omega$

In the region shown, one could use source transformation twice and reduce that part to a single source with a resistor.

... Or we can apply Thevenin Equivalence to that part (viewed as "Part A")

$$R_{TH} = 4k\Omega$$

For the open loop voltage the part outside the region is eliminated

$$V_{TH} = \frac{6}{3+6} 12[V] = 8[V]$$

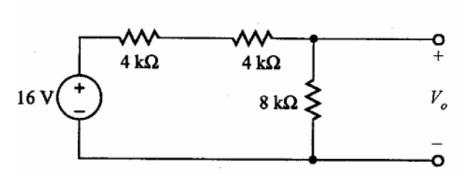
And one can apply Thevenin one more time!

For open loop voltage use KVL

$$R^1_{TH} = 4k\Omega$$

$$V_{TH}^1 = 4k * 2mA + 8V = 16V$$

...and we have a simple voltage divider!!

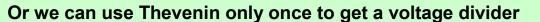


$$V_0 = \frac{8}{8+8} 16[V] = 8V$$

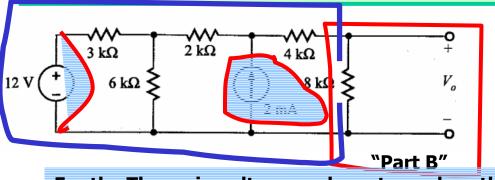


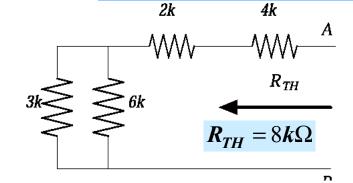






For the Thevenin resistance





For the Thevenin voltage we have to analyze the following circuit

METHOD??

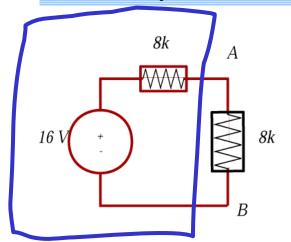
Source superposition, for example

$$V_{OC}^1 = \frac{6}{3+6} 12V = 8V$$

Thevenin Equivalent of "Part A"

Contribution of the current source

$$V_{OC}^2 = (2k + 2k)*(2mA) = 8V$$



Simple Voltage Divider

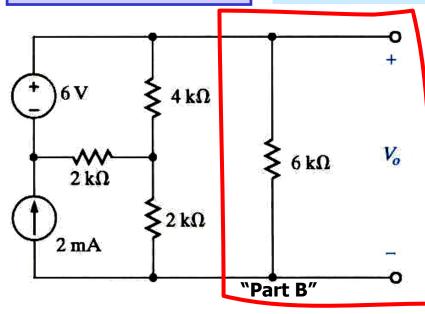






LEARNING EXAMPLE

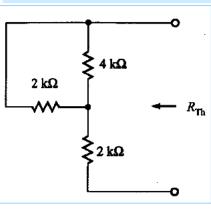
USE THEVENIN TO COMPUTE Vo

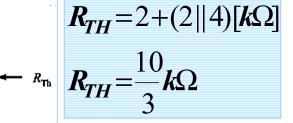


You have the choice on the way to partition the circuit.

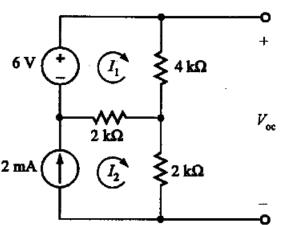
Make "Part A" as simple as possible

Since there are only independent sources, for the Thevenin resistance we set to zero all sources and determine the equivalent resistance





For the open circuit voltage we analyze the following circuit ("Part A") ...



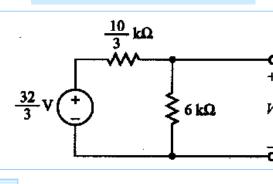
Loop Analysis

$$I_2 = 2mA$$

$$-6V + 4kI_1 + 2k(I_1 - I_2) = 0$$

$$I_1 = \frac{6 + 2I_2}{6} mA = \frac{5}{3} mA$$

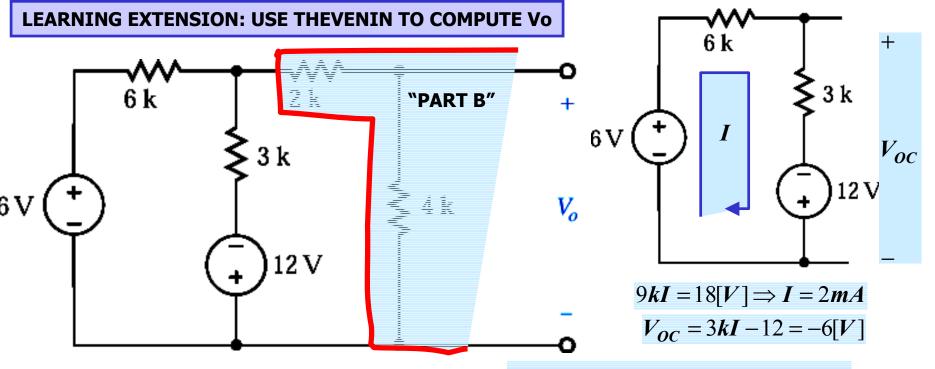
The circuit becomes...

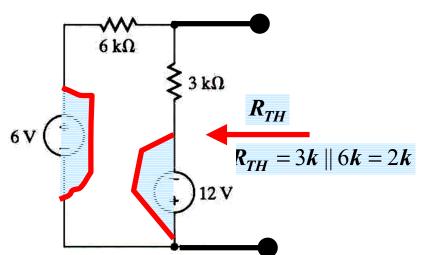


$$V_{OC} = 4k * I_1 + 2k * I_2 = 20/3 + 4V = 32/3[V]$$









RESULTING EQUIVALENT CIRCUIT

$$R_{TH} = 2k\Omega \quad 2k\Omega$$

$$V_{TH} = -6V$$

$$V_{TH} = -6V$$

$$V_{TH} = -6V$$

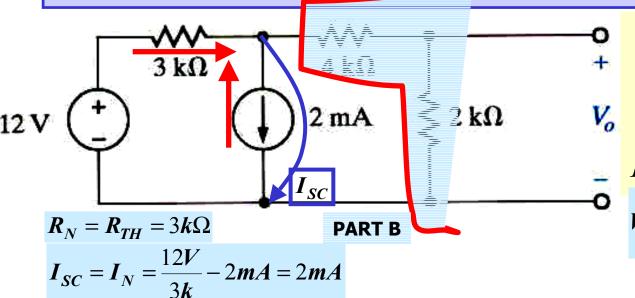
$$V_o = \frac{4}{4+4}(-6V) = -3[V]$$







LEARNING EXTENSION: COMPUTE Volusing NORTON

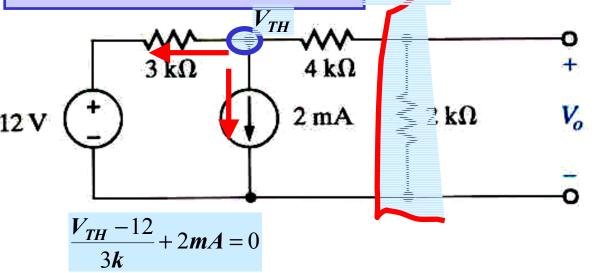


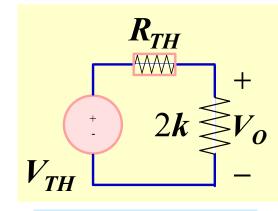
$$V_{O} = 2kI = 2k \left(\frac{R_{N}}{R_{N} + 6k}I_{N}\right)$$

$$V_o = 2\frac{3}{9}(2) = \frac{4}{3}[V]$$

COMPUTE Vo USING THEVENIN PART B

 $R_{TH} = 3k + 4k$





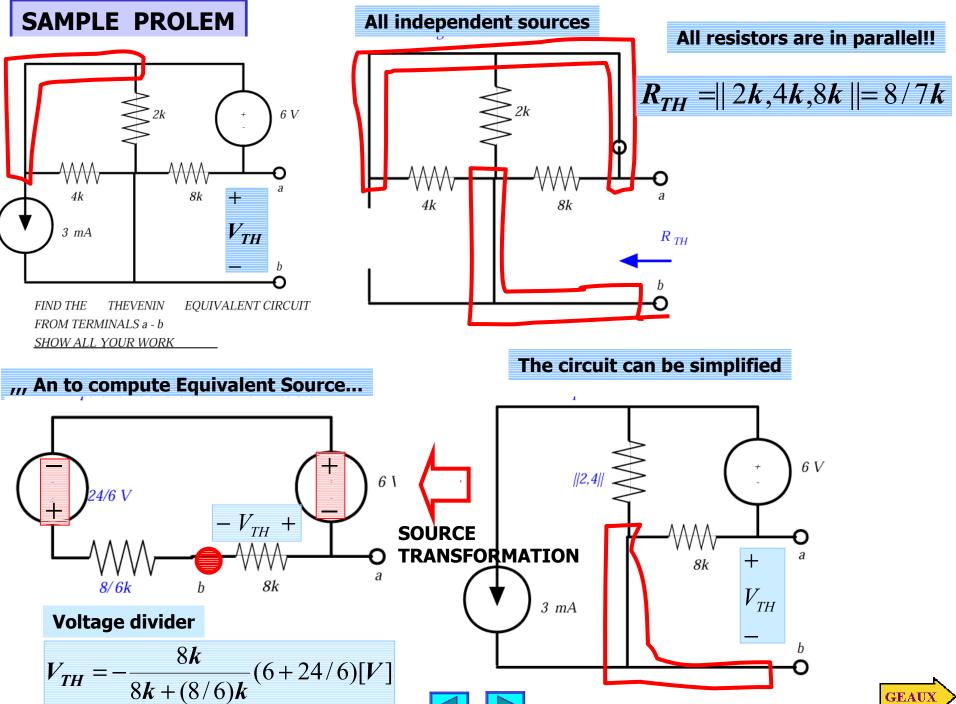
$$V_o = \frac{2}{2+7}(6V) = \frac{4}{3}[V]$$



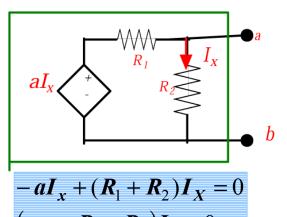




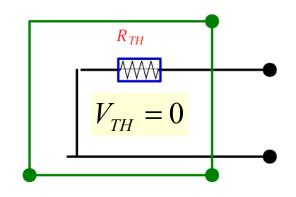
SAMPLE PROBLEM Equivalent Resistance: Independent sources only FIND THE THEVENIN EQUIVALENT AT a - b R_{TH} $V_{\mathcal{S}}$ I_{S} $R_{TH} = 3R || 3R = 1.5R$ V_{TH} **Equivalent Voltage: Node, loop, superposition...** Do loops **KVL** $I_1 = I_S$ $-V_S + 5R(I_1 + I_2) + RI_2 = 0$ $V_{TH} = -RI_2 - 2R(I_1 + I_2)$ **How about source superposition?** $V_{TH}^1 = -\frac{V_S}{2}$ **Opening the current source:** R_{TH} Short circuiting the voltage source V_{TH} $I_1 = \frac{5}{6}I_S I_2 = \frac{1}{6}I_S$ $V_{TH}^2 = RI_1 - 2RI_2 = \frac{1}{2}RI_S$ This is what we need to get KVL $V_{TH} = V_{TH}^1 + V_{TH}^2$ **GEAUX**



THEVENIN EQUIVALENT FOR CIRCUITS WITH ONLY DEPENDENT SOURCES



$$(-\mathbf{a} + \mathbf{R}_1 + \mathbf{R}_2)\mathbf{I}_x = 0$$
$$-\mathbf{a} + \mathbf{R}_1 + \mathbf{R}_2 \neq 0 \Rightarrow \mathbf{I}_x = 0$$



A circuit with only dependent sources cannot self start.

(actually that statement has to be qualified a bit. What happens if $a = R_1 + R_2$?)

FOR ANY PROPERLY DESIGNED CICUIT WITH ONLY DEPENDENT SOURCES $V_{OC}=0,\,I_{SC}=0$

This is a big simplification!!

But we need a special approach for the computation of the Thevenin equivalent resistance

Since the circuit cannot self start we need to probe it with an external source

The source can be either a voltage source or a current source and its value can be chosen arbitrarily!

Which one to choose is often determined by the simplicity of the resulting circuit

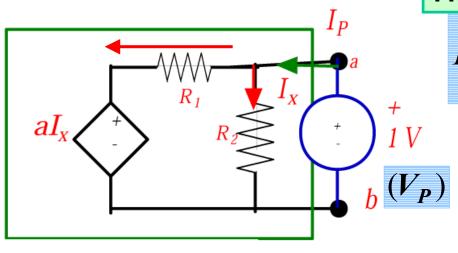






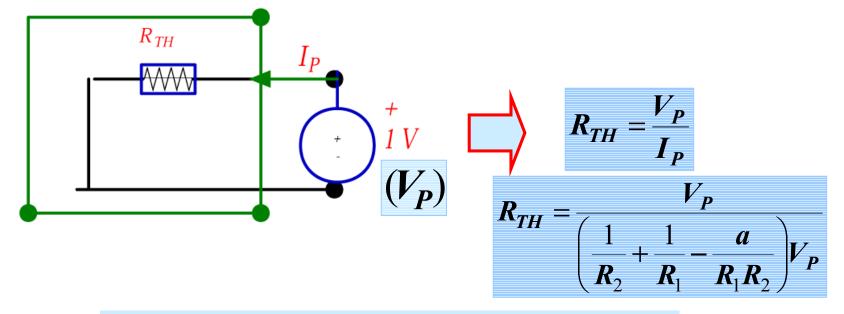
IF WE CHOOSE A VOLTAGE PROBE...

WE MUST COMPUTE CURRENT SUPPLIED BY PROBE SOURCE



$$I_P = I_X + \frac{V_P - aI_X}{R_1} \qquad I_X = \frac{V_P}{R_2}$$

$$\boldsymbol{I}_{\boldsymbol{P}} = \left(\frac{1}{\boldsymbol{R}_2} + \frac{1}{\boldsymbol{R}_1} - \frac{\boldsymbol{a}}{\boldsymbol{R}_1 \boldsymbol{R}_2}\right) \boldsymbol{V}_{\boldsymbol{P}}$$



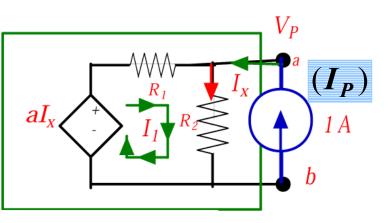
The value chosen for the probe voltage is irrelevant. Oftentimes we simply set it to one







IF WE CHOOSE A CURRENT SOURCE PROBE



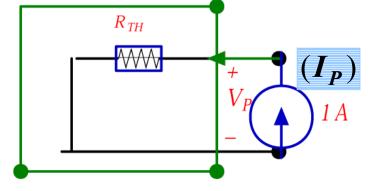
We must compute the node voltage V_p

KCL

$$\frac{\boldsymbol{V_P}}{\boldsymbol{R}_2} + \frac{\boldsymbol{V_P} - a\boldsymbol{I}_X}{\boldsymbol{R}_1} - \boldsymbol{I}_P = 0$$

$$I_X = \frac{V_P}{R_2}$$

$$\left(\frac{1}{R_2} + \frac{1}{R_1} - \frac{a}{R_1 R_2}\right) V_P = I_P$$





$$R_{TH} = \frac{V_P}{I_P}$$

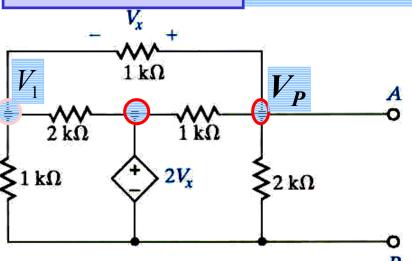
The value of the probe current is irrelevant. For simplicity it is often choosen as one.







LEARNING EXAMPLE | FIND THE THEVENIN EQUIVALENT



Do we use current probe or voltage probe?

If we use voltage probe there is only one node not connected through source

$$KCL@V_1: \frac{V_1}{1k} + \frac{V_1 - 2V_X}{2k} + \frac{V_1 - V_P}{1k} = 0$$

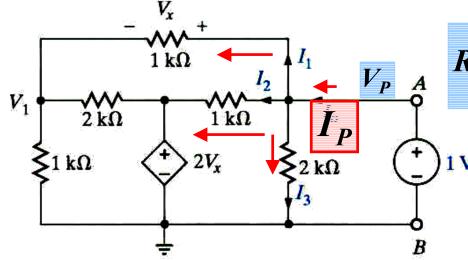
Controlling variable: $V_X = V_P - V_1$

SOLVING THE EQUATIONS

$$V_1 = \frac{4}{7}V_P, \qquad V_X = \frac{3}{7}V_P$$

$$I_{P} = \frac{V_{P}}{2k} + \frac{V_{P} - 2V_{X}}{1k} + \frac{V_{X}}{1k}$$

$$I_{P} = \frac{15V_{P}}{14k}$$



$$R_{TH} = \frac{V_P}{I_P} = \frac{14}{15} k\Omega$$

Using voltage probe. Must compute 1 v current supplied

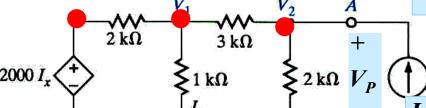


LEARNING EXAMPLE Find the Thevenin Equivalent circuit at A - B Only dependent sources. Hence V_th = 0 $\frac{N}{2 \text{ k}\Omega}$ $3 k\Omega$ 2000 I, $1 \, k\Omega$ $2 k\Omega$

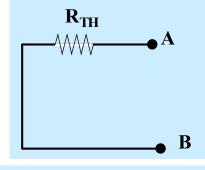


@V_2

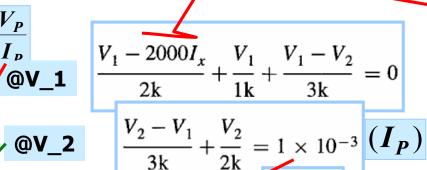




"Conventional" circuit with dependent sources - use node analysis



Thevenin equivalent



Controlling variable $I_x =$

$$3(V_1 - 2V_1) + 6V_1 + 2(V_1 - V_2) = 0$$

$$2(V_2 - V_1) + 3V_2 = 6[V]$$

$$V_1 - 2V_2 = 0$$
 * / 2

$$-2V_1 + 5V_2 = 6 * / 5$$

$$5V_1 - 2V_2 = 0 - 2V_1 + 5V_2 = 6 * / 5 V_2 = \frac{30}{21} = \frac{10}{7}$$

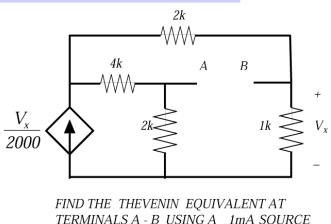
$$(V_P = V_2) \cap (I_P = 1 mA) \Rightarrow R_{TH} = \frac{V_2}{1 mA} = (10/7) k\Omega$$

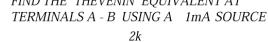


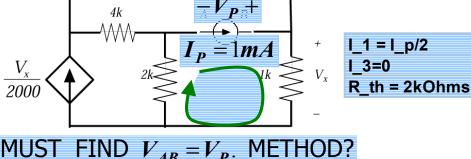




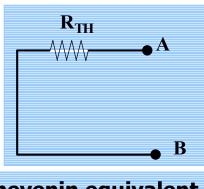
SAMPLE PROBLEM







MUST FIND $V_{AB} = V_{P}$. METHOD?

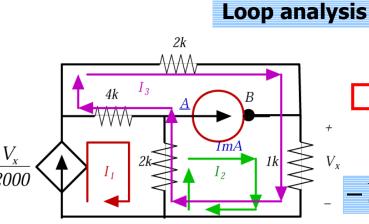


Thevenin equivalent



$$R_{TH} = \frac{V_P}{I_P} = \frac{V_P}{1mA}$$

The resistance is $P = V_P$ numerically equal to V_p but with units of KOhm



$$I_1 = \frac{V_X}{2000}; I_2 = I_P$$

 $2k * I_3 + 1k * (I_2 + I_3) + 2k * (I_3 + I_2 - I_1) + 4k * (I_3 - I_1) = 0$

Controlling variable $V_X = 1k * (I_3 + I_2)$

Voltage across current probe

 $-V_P + 1k*(I_3 + I_2) + 2k*(I_3 + I_2 - I_1) = 0$







Thevenin Equivalent Circuits with both Dependent and Independent Sources

We will compute open circuit voltage and short circuit current

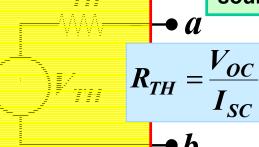
LINEAR CIRCUIT

May contain
independent and
dependent sources
with their controlling
variables
PART A

For each determination of a Thevenin equivalent we will solve two circuits

Any and all the techniques discussed should be readily available; e.g.,

KCL, KVL, combination series/parallel, node, loop analysis, source superposition, source transformation, homogeneity



vo

 \boldsymbol{b}

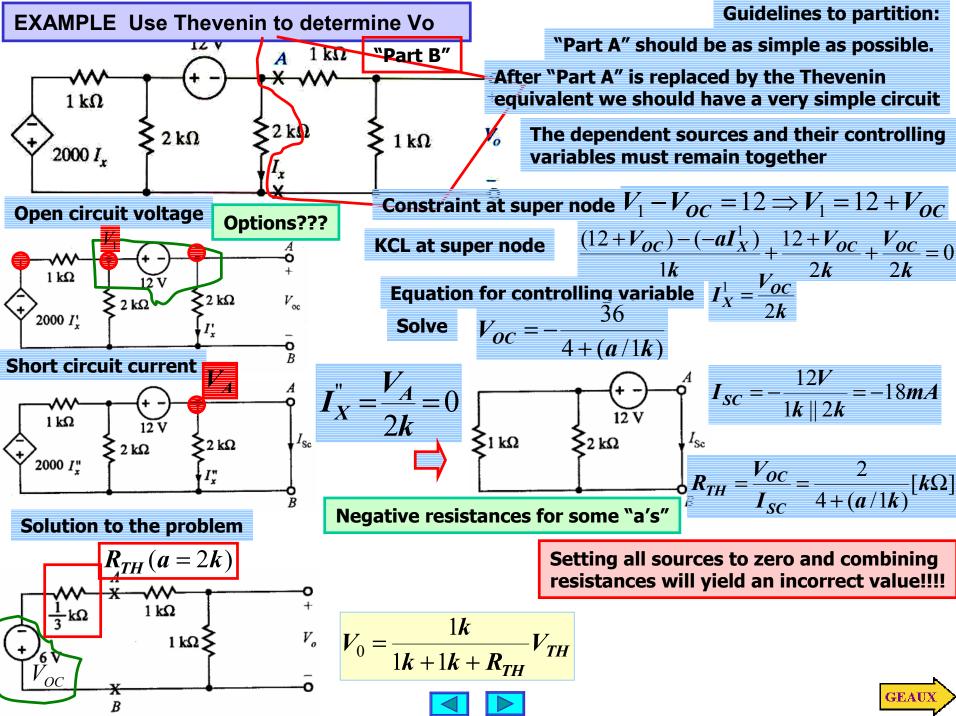
$$V_{TH} = V_{OC}$$

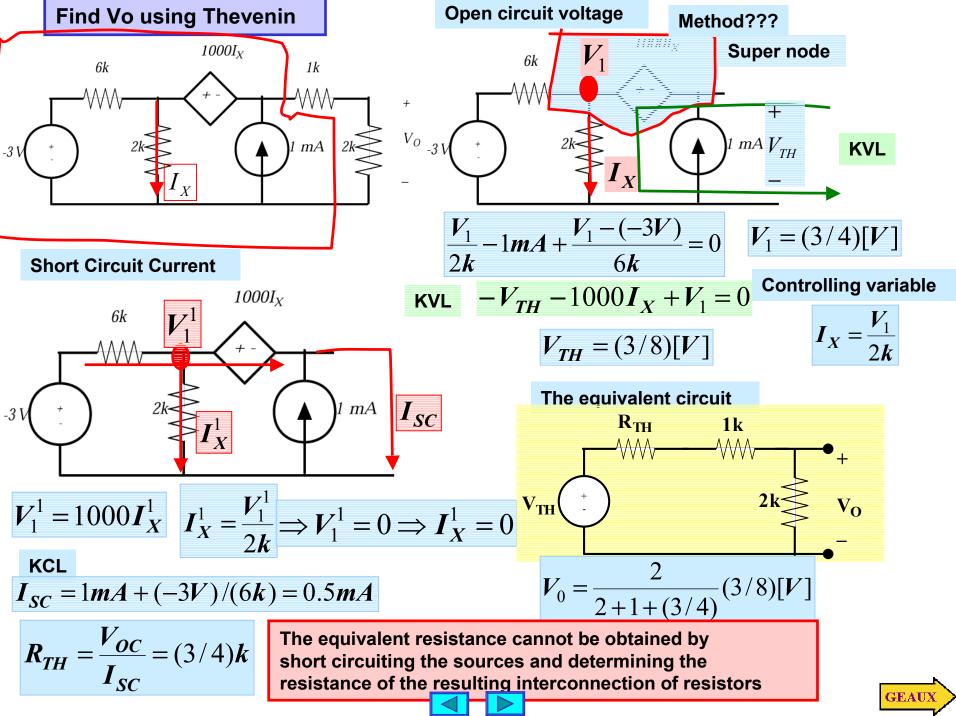
The approach of setting to zero all sources and then combining resistances to determine the Thevenin resistance is in general not applicable!!

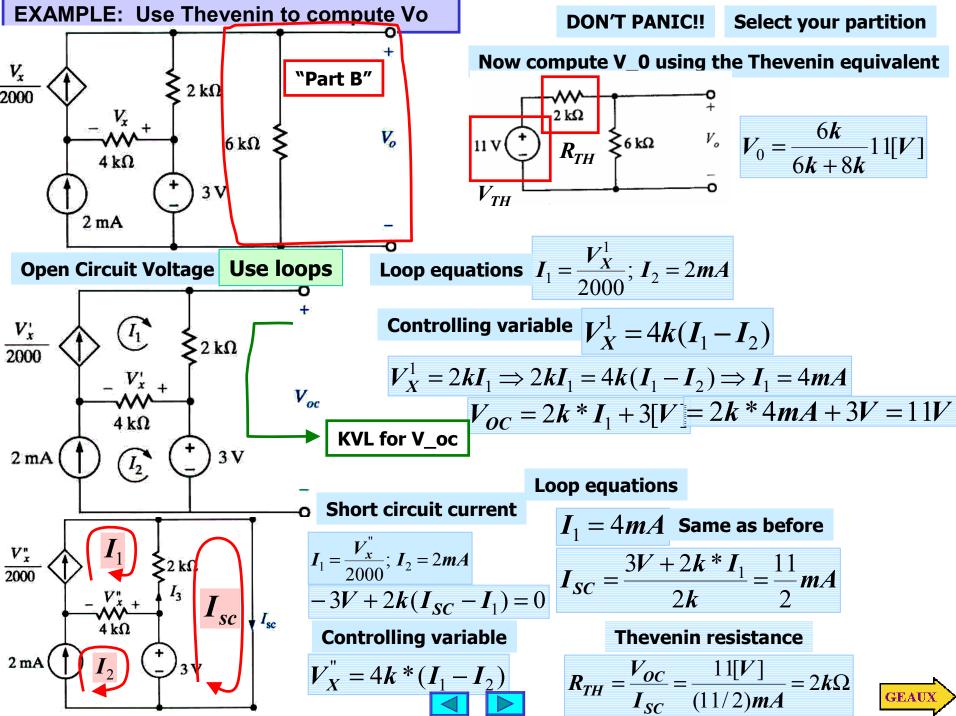




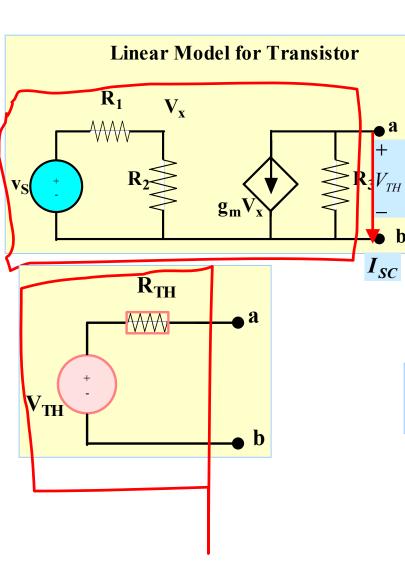








EXAMPLE



The alternative for mixed sources

$$V_{TH} = V_{OC}, \quad R_{TH} = \frac{V_{OC}}{I_{SC}}$$

Open circuit voltage

$$V_{TH} = -g_m R_3 V_x$$

$$V_x = \frac{R_2}{R_1 + R_2} v_S \Rightarrow V_{TH} = -g_m \frac{R_3 R_2}{R_1 + R_2} v_S$$

Short circuit current

$$I_{SC} = -g_m V_x = -g_m \frac{R_2}{R_1 + R_2} v_S$$

Equivalent Resistance

$$R_{TH} = \frac{V_{OC}}{I_{SC}} = R_3$$

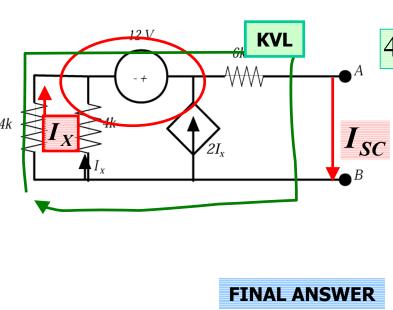






SAMPLE PROBLEM supernode 6k 12V TH A FIND THE THEVENIN EQUIVALENT AT THE TERMINALS A - B

Short circuit current



Mixed sources. Must compute Voc and Isc

Open circuit voltage

KCL at super node
$$\boldsymbol{I}_1 + \boldsymbol{I}_X + 2\boldsymbol{I}_X = 0$$

The two 4k resistors are in parallel $oldsymbol{I}_1 = oldsymbol{I}_X$

$$I_X = 0 \Rightarrow V_{TH} = 12[V]$$

KCL at supernode

$$I_{SC} = 4I_X$$

$$4k*(I_{SC}/4)-12[V]+6k*I_{SC}=0$$

$$R_{TH} = \frac{V_{TH}}{I_{SC}} = \frac{12V}{(12/7)mA} = 7k\Omega$$



SAMPLE PROBLEM FIND THE THEVENIN EQUIVALENT AT a - b Short circuit current We need to compute V x Single node KCL@Vx $\frac{V_X^1 - 2V_S}{2R} + \frac{V_X^1}{R} - aV_X^1 + \frac{V_X^1 - V_S}{2R} = 0$ $\Rightarrow V_X^1 = \frac{3V_S}{4 - 2aR}$

 $R_{TH} = \frac{V_{OC}}{I_{GC}} = \frac{V_{TH}}{I_{GC}} = \frac{4R(1-2aR)}{3}$

Mixed sources! Must compute open loop voltage and short circuit current Open circuit voltage

$$V_{TH} = V_X - V_b$$

For Vx use voltage divider

$$V_X = \frac{R}{R + 2R} (2V_S) = \frac{2}{3} V_S$$

 $V_{TH} = -\frac{1 + 4aR}{2}V_S$

For Vb use KVL

$$Z = 2D(aV)$$

 R_{TH}

-

 $V_{h} = 2R(aV_{x}) + V_{s} = (1 + 4aR/3)V_{s}$

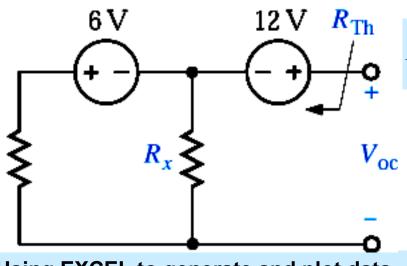
 $V_{TH} = V_X - (2RaV_X + V_S) = (1 - 2Ra)(2V_S/3) - V_S$

KCL again can give the short circuit current

 $I_{SC} = -aV_X^1 + \frac{V_X^1 - V_S}{2R}$ $I_{SC} = -\frac{1 + 4aR}{4R(1 - 2aR)}V_S$

_ a FINAL ANSWER

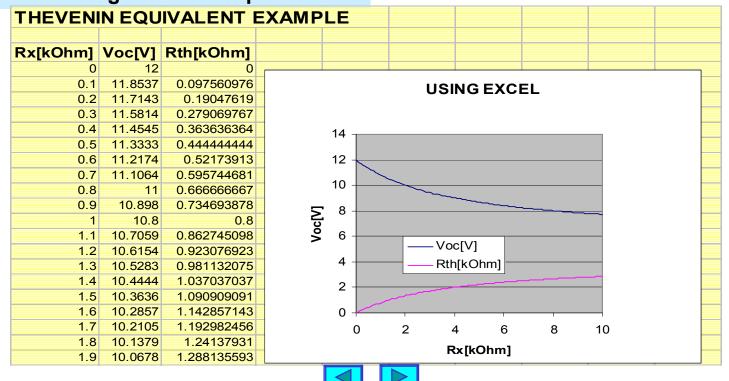
LEARNING EXAMPLE FIND AND PLOT R_{TH} , V_{OC} , WHEN $0 \le R_X \le 10 k\Omega$



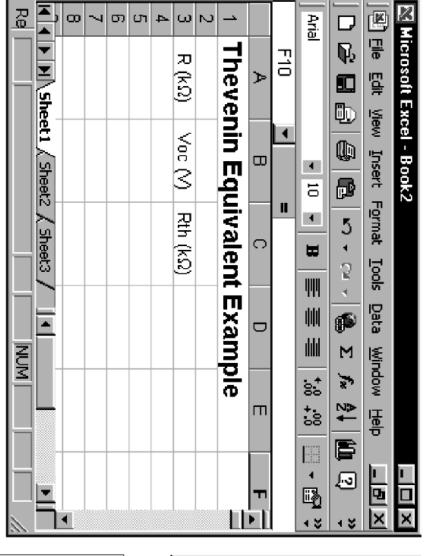
DATA TO BE PLOTTED

$$R_{TH} = 4k \parallel R_X = \frac{4R_X}{4 + R_X}$$
 $V_{OC} = 12 - 6 \left[\frac{R_X}{4k + R_X} \right]$

Using EXCEL to generate and plot data

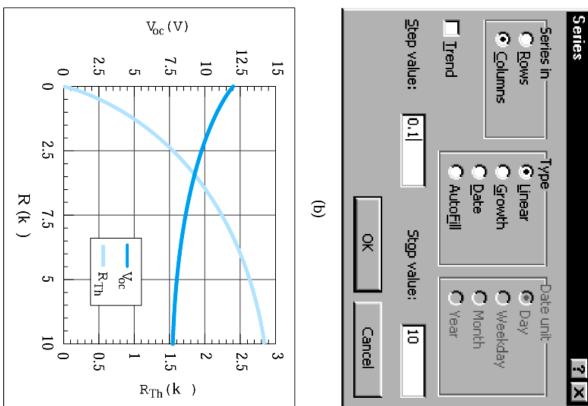




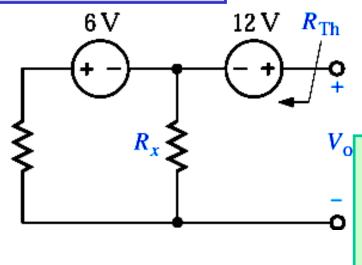


(a)

<u>C</u>



LEARNING EXAMPLE FIND AND PLOT R_{TH} , V_{OC} , WHEN $0 \le R_X \le 10k\Omega$

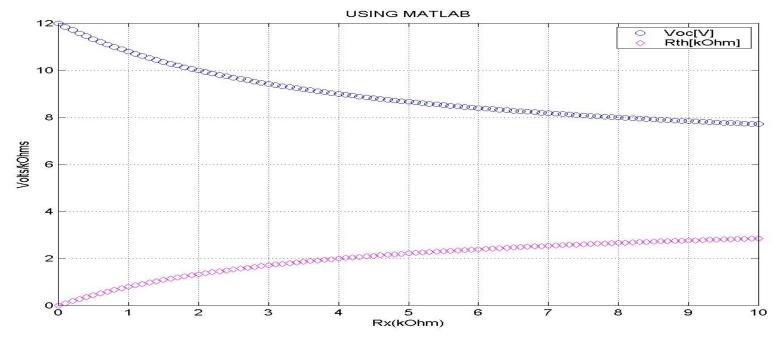


DATA TO BE PLOTTED

$$R_{TH} = 4k \parallel R_X = \frac{4R_X}{4 + R_X}$$
 $V_{OC} = 12 - 6 \left[\frac{R_X}{4k + R_X} \right]$

Using MATLAB to generate and plot data

- » Rx=[0:0.1:10]'; %define the range of resistors to use
- » Voc=12-6*Rx./(Rx+4); %the formula for Voc. Notice "./"
- » Rth=4*Rx./(4+Rx); %formula for Thevenin resistance.
- » plot(Rx,Voc,'bo', Rx,Rth,'md')
- » title('USING MATLAB'), %proper graphing tools
- » grid, xlabel('Rx(kOhm)'), ylabel('Volts/kOhms')
- » legend('Voc[V]','Rth[kOhm]')

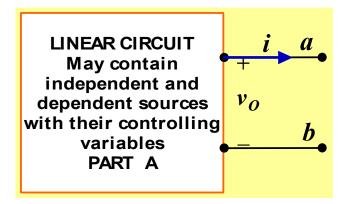


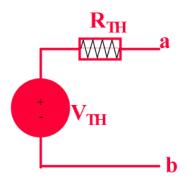




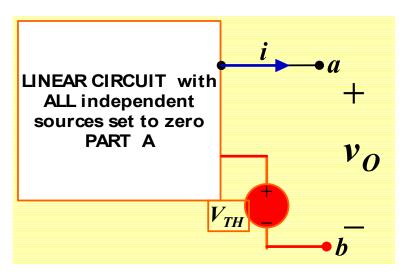


A MORE GENERAL VIEW OF THEVENIN THEOREM

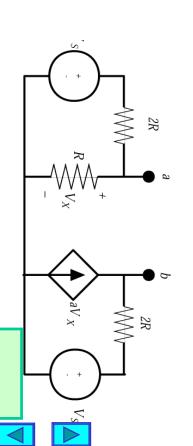


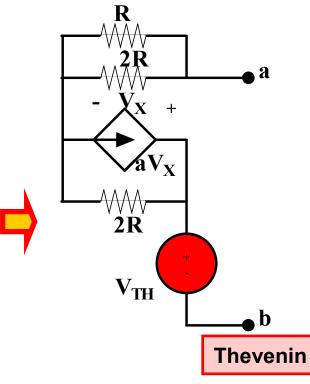


USUAL INTERPRETATION

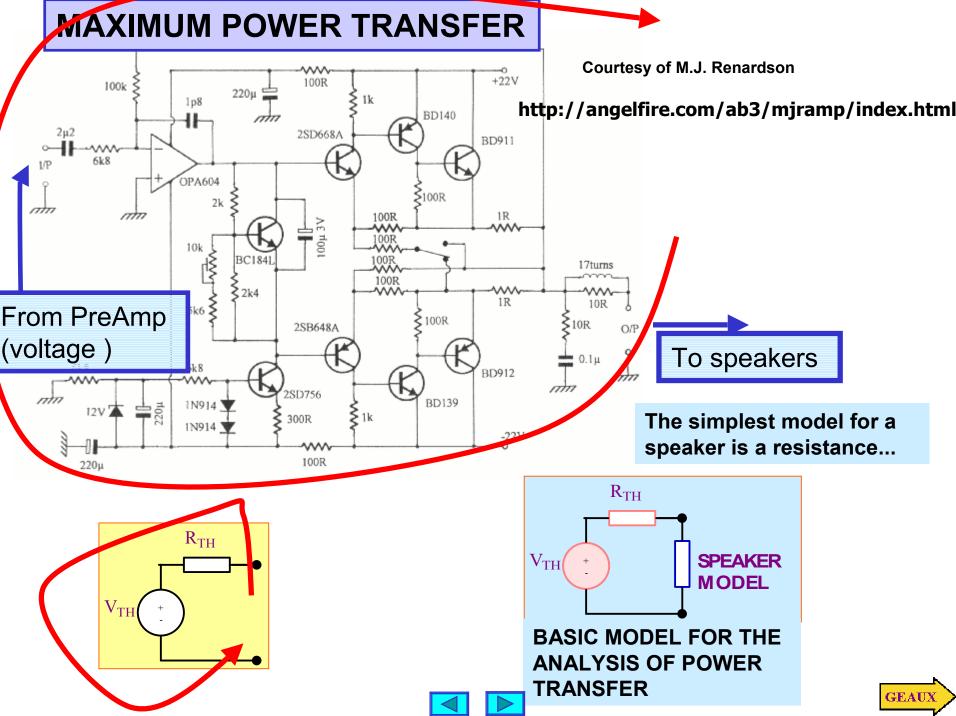


THIS INTERPRETATION APPLIES
EVEN WHEN THE PASSIVE ELEMENTS
INCLUDE INDUCTORS AND CAPACITORS

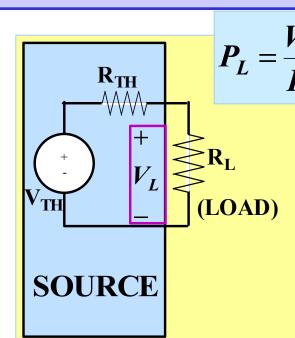








MAXIMUM POWER TRANSFER



$$P_{L} = \frac{V_{L}^{2}}{R_{L}}; V_{L} = \frac{R_{L}}{R_{TH} + R_{L}} V_{TH}$$

$$P_{L} = \frac{R_{L}}{(R_{TH} + R_{L})^{2}} V_{TH}^{2}$$

For every choice of R_L we have a different power. How do we find the maximum value?

Consider P L as a function of R L and find the maximum of such function

$$\frac{dP_L}{dR_L} = V_{TH}^2 \left(\frac{(R_{TH} + R_L)^2 - 2R_L(R_{TH} + R_L)}{(R_{TH} + R_L)^4 - 3} \right)$$

Technically we need to verify that it is indeed a maximum

Set the derivative to zero to find extreme points. For this case we need to set to zero the numerator

$$R_{TH} + R_L - 2R_L = 0 \Rightarrow R_L^* = R_{TH}$$
 The maximum power transfer theorem

The value of the maximum power that can be

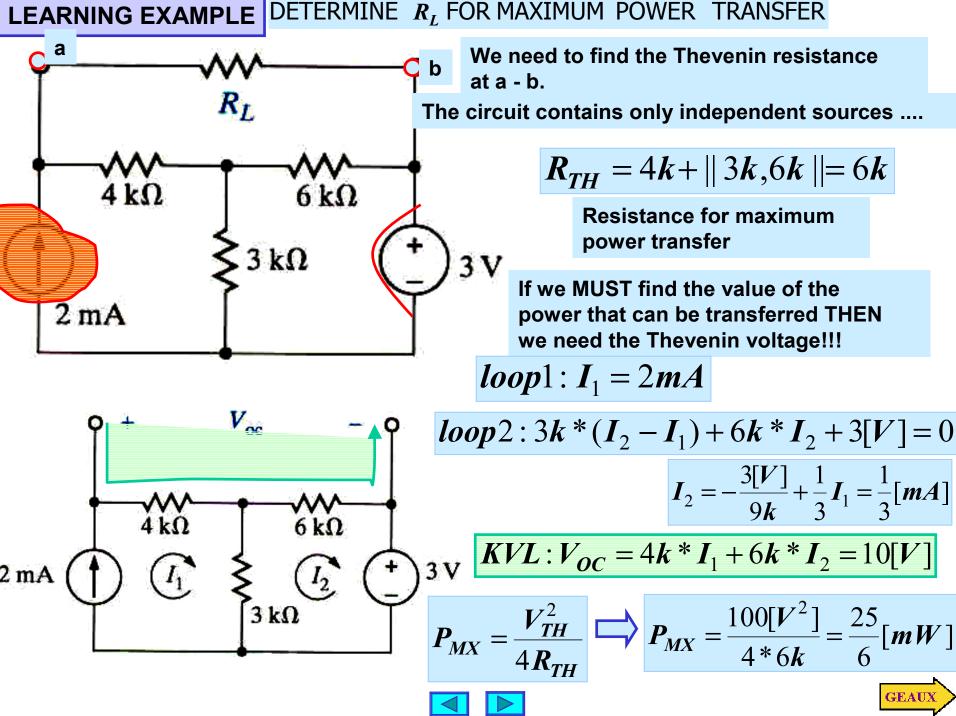
The load that maximizes the power transfer for a circuit is equal to the Thevenin equivalent resistance of the circuit.

transferred is









LEARNING EXAMPLE DETERMINE R_L AND MAXIMUM POWER TRANSFERRED $4 k\Omega$ 1. Find the Thevenin equivalent at a - b



transfer

2. Remember that for maximum power transfer
$$R_L = R_{TH}$$
 $P_{MX} = \frac{V_{TH}^2}{4R_{TH}}$

b

.... And it is simpler if we do Thevenin at c - d and account for the 4k at the end

$$loop1: I_1 = 4mA$$

 $loop 2: -2kI_X + 2kI_2 + 4k(I_2 - I_1) = 0$

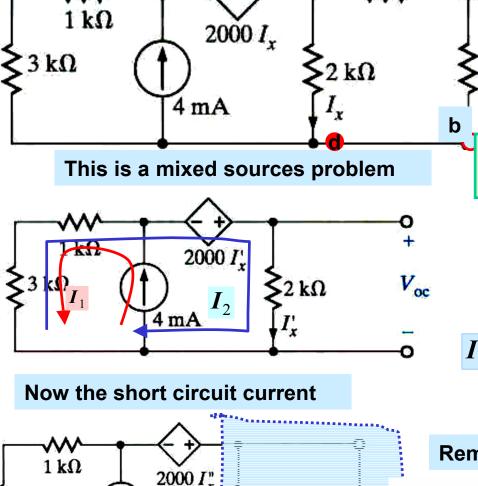
Controlling variable: $I_X = I_2$

$$- \Lambda_{100} \Lambda \rightarrow I / - 9 \Gamma I / 1$$

$$I_{2} = I_{1} = 4mA \Rightarrow V_{OC} = 8[V]$$

$$I''_{X} = 0 \Rightarrow I_{SC} = 4mA$$

Remember now where the partition was made



3 kΩ

4 mA

8V

 $2 k\Omega$

 $R_I = 6k$

 $4 k\Omega$